PHILIPS

PRM80 SERIES VHF/UHF MOBILE

WARNING

The transistors used in the transmitter power amplifier contain beryllium oxide, the dust of which Is toxic.

No danger can arise from normal handling, but no attempt should be made to tamper with the encapsulation of these devices. They must not be discarded with Industrial or domestic waste.

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SECTION 1 INTRODUCTION

1.1 PRODUCT DESCRIPTION

The PRM80 series of mobile radio transceivers are primarily, under dash mounted local controlled simplex radios, for vehicular application.

The design concept utilises an advanced microcomputer controlled frequency synthesizer. The microcomputer also performs analogue signalling. The selective calling systems provided meet the requirements of both standard despatch communications and special systems applications in world-wide private mobile radio markets.

In addition to the tone sequential signalling, continuous tone controlled squelch system (CTCSS) signalling is provided and includes the reverse tone burst encode feature.

The customization of the microcomputer control is via an electrically erasable programmable read only memory (EEPROM). The mobile radio may be configured to meet specific customer requirements by programming the EEPROM via the data port available at the microphone socket.

An innovative receiver design provides full band coverage without the need for mechanical tuning. Similarly, a range of broadband transmitter power amplifiers, offering a selection of power output levels, provide full band coverage without the need to mechanically re-tune. The local control front panel is available in two versions. One version provides up to 9 channels and control of a limited set of software programmable options. The other version provides up to 64 channels, and additional buttons and display indicators give the operator access to a more comprehensive range of features. Both front panels utilise liquid crystal displays with permanent backlighting.

The PRM80 is constructed with extensive use of miniature surface mounted components.

The compact electro-mechanical design interconnects the various circuit functions without the use of point to point wiring, making the PRM80 a true "wireless" radio.

1.1.1 Product Variants

The main unit of the **PRM80** transceiver is available in a number of uniquely configured hardware variants. These variant related items are listed below.

i)	Channel Capacity	9-channel or 64-channel (Different front panel and memory capacity).

ii)	Transmitter Power	1 to 6 watt, 1 to 25 watt, 10 to 40 watt. (Different printed circuit board assemblies required for each option).
iii)	Frequency Band	EO band, A9 band/BO band, Tm band, UO band, W 1 band, W4 band. (Different printed circuit board assemblies required for each band).
iv)	Channel Spacing	12.5kHz, 20kHz, 25/30kHz. (Different printed circuit board assemblies required for each option).
v)	Frequency Stability:	+/-5 ppm -10 to +60 Deg C (Better quality crystal). +/-10 ppm -10 to +60 Deg C (Standard crystal). +/-5 ppm -30 to +60 Deg C (Extended temp option). +/-2.5 ppm -10 to +60 Deg C (TXCO). +/-2.5 ppm -30 to +60 Deg C (TCXO) +/-10 ppm -30 to +60 Deg C (Extended temp option)
vi)	Receiver Mute	Adjustable/Preset. (Additional components required on printed circuit board).
vii)	Signalling	- Without CTCSS encoder/decoder - With CTCSS encoder/decoder (Additional components on printed circuit board). - Standard Selcall - High performance Selcall (Additional components on printed circuit board).
viii)	Systems:	- Standard no systems interface - Systems interface. (Additional components on printed circuit board).

1.1.2 Product Family

The PRM80 is provided with a family of product related ancillaries for standard vehicular installation and base or office environment application.

The ancillaries are:

i) Desk top housing with mains power supply.

ii) Stand microphone.

iii) Boom microphone.

iv) Hands-free microphone.

v) Small loudspeaker.

vi) Large loudspeaker

vii) Depot Data programmer.

viii) 24 volt to 12 volt do to do converter.

ix) Interference filter (12 volt do power).

1.2 MECHANICAL CONSTRUCTION

The main transceiver unit contains **three printed circuit boards.** Each are double sided epoxy fibreglass with plated through holes. Extensive use is made of surface mounted components but conventional leaded components are also used.

The three printed circuit boards are defined as:

i) FRONT PANEL

ii) CONTROL

iii) RADIO

An aluminium diecast chassis provides for heat sinking of the power amplifiers and regulator devices. The radio and control PCBs are attached to this and are shielded from each other by a central partition which is part of the main casting. The radio PCB has a separate zinc die cast shield which is fitted on the component assembly side. This shield effectively compartmentalizes circuit function areas on the radio PCB. Interconnection between the radio and control PCBs is via a flexible printed circuit with a zero insertion force socket fitted to the radio PCB.

Interconnection from the control PCB to the front panel PCB is via a flexible printed circuit with a zero insertion force socket fitted to the front panel PCB. No wiring looms are used in the mechanical assembly.

A moulded plastic sleeve provides a styling cover over the PCB and chassis assembly. The front panel PCB is housed in a separate plastic moulding.

In the 9-channel front panel, four moulded plastic buttons are clipped in as part of the front panel moulding. A clear plastic lens welded to the front panel moulding provides protection for the liquid crystal display. Behind the LCD is a light diffuser lens to aid in back lighting and location of the LCD electrical connector (zebra strip). Placed between the front panel moulding and the front panel PCB is a moulded rubber mat containing the switch contact pads and this mat also aids in location of the complete LCD/Diffuser/Zebra Strip assembly.

The 64-channel front panel is similar in construction to the 9-channel version, however, 8 buttons are provided which are clipped into the moulded assembly. The LCD is retained on the front panel printed circuit board assembly by a pressed metal frame. This frame also retains the switch rubber mat and LCD diffuser assembly.

The front panel PCBs are attached to the front panel moulding by fixing screws.

The front panel assembly is attached to the outer sleeve and a dust and water seal gasket is provided at this interface.
The antenna connection is provided by a chassis mounted BNC type socket at the rear of the main chassis. Connection to the loud speaker and do power is provided by a 4-way connector socket mounted on the control PCB, and is accessed at the rear of the main chassis. For special systems applications, a 15-way 'D' type connector is mounted on the rear of the chassis and connected internally via a ribbon cable and plug to the control PCB.
The microphone socket is mounted on the control PCB and is accessed via an opening in the front panel moulding. A clip-on moulded plastic facade covers the microphone socket connection.

The installation mounting cradle is fixed to the central partition section of the main chassis. Two fixing screws remain attached to the chassis and secure the outer sleeve in position. The cradle is secured in position by two more screws. Tilt adjustment of the cradle mounting is set before the screws are finally tightened.

1.3 SERVICE/ACCESSIBILITY

To gain access to the PCB assemblies the front panel must be detached first (microphone, knob, one fixing screw, one lock nut and disconnect the flexible printed circuit from the front panel). The outer sleeve is then removed (four fixing screws). The front panel may be re-attached to the control PCB with the flexible PCB/socket interconnection. At this level of assembly the equipment may be operated and aligned. Access to the component side of the control PCB is possible. The majority of the components on this board are surface mounted and may be serviced with the PCB in-situ.

To gain access to the radio PCB the radio screen must be detached (nine fixing screws). The equipment may be operated at this level of assembly but with degraded performance in terms of case radiation and spurious response and emissions. For service, access to the component side is possible . The majority of the components on the radio PCB are surface mounted and may be serviced with the PCB in-situ.
For access to the underside of the radio PCB three fixing screws must be removed, fixing screws on the transmitter power amplifier devices must also be removed (6 for UHF 25W & 40W, 4 for the UHF 6W version, 3 for the VHF 6W & 25W, and 5 for the 40W VHF version). The antenna socket connection must be de-soldered and the 13 volt power connection at the chassis feed through must be de-soldered. The radio board may then be detached from the chassis but will remain connected to the control PCB by the flexible interconnecting circuit. This flexible PCB may be disconnected at the socket on the radio board.

For access to the underside of the control PCB the front panel must be detached. The microphone must also be removed. The control PCB is retained by six fixing screws, the audio amplifier IC and two regulator ICs are attached to the chassis by four fixing screws which must be removed. The 13 volt power connection at the chassis feed through must be de-soldered.

The control board may then be removed from the chassis but it remains connected to the radio PCB and front panel by a flexible interconnecting circuit-Care must be exercised when re-attaching a control PCB to the chassis, to ensure that the 5V regulator, IC208, has the insulating washer and bush correctly fitted. Similarly, when re-attaching the radio PCB

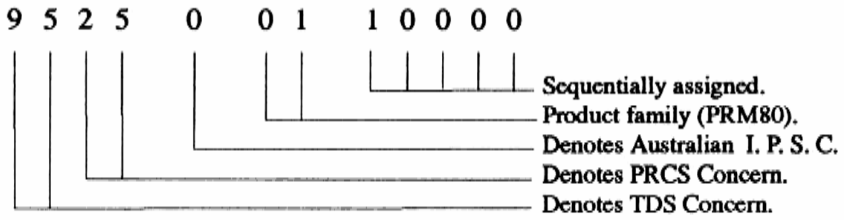
to the chassis, care must be exercised to ensure that the transmitter power amplifier devices have the correct amount of heatsink compound applied to their mounting faces before fixing to the chassis.

Should the interconnecting flexible printed circuit fail, a hand solderable replacement alternative is available. The factory fitted flex strip must first be carefully removed from the control PCB, by applying a "hot air" de-soldering tool to the solder joint and peeling away the soldered connections.

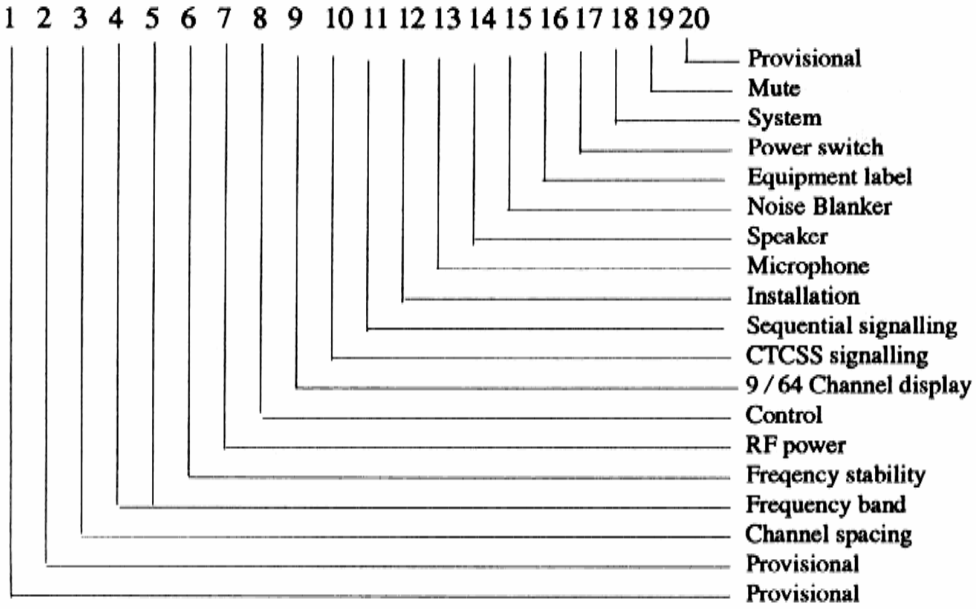
1.4 SALES CODES

There are, basically, two codes to be described; the 12-digit sales code and the 20-digit supplementary technical code. A sample of this latter code sheet is included.

1.4.1 The 12-digit Sales Code


9 5 2 5 0 0 1 1 0 0 0 0
Sequentially assigned.
Product family (PRM80).
Denotes Australian I. P. S. C.
Denotes PRCS Concern.
Denotes TDS Concern.

1.4.2 The 20-digit Supplementary Technical Code



PRM80 SUPPLEMENTARY TECHNICAL CODE

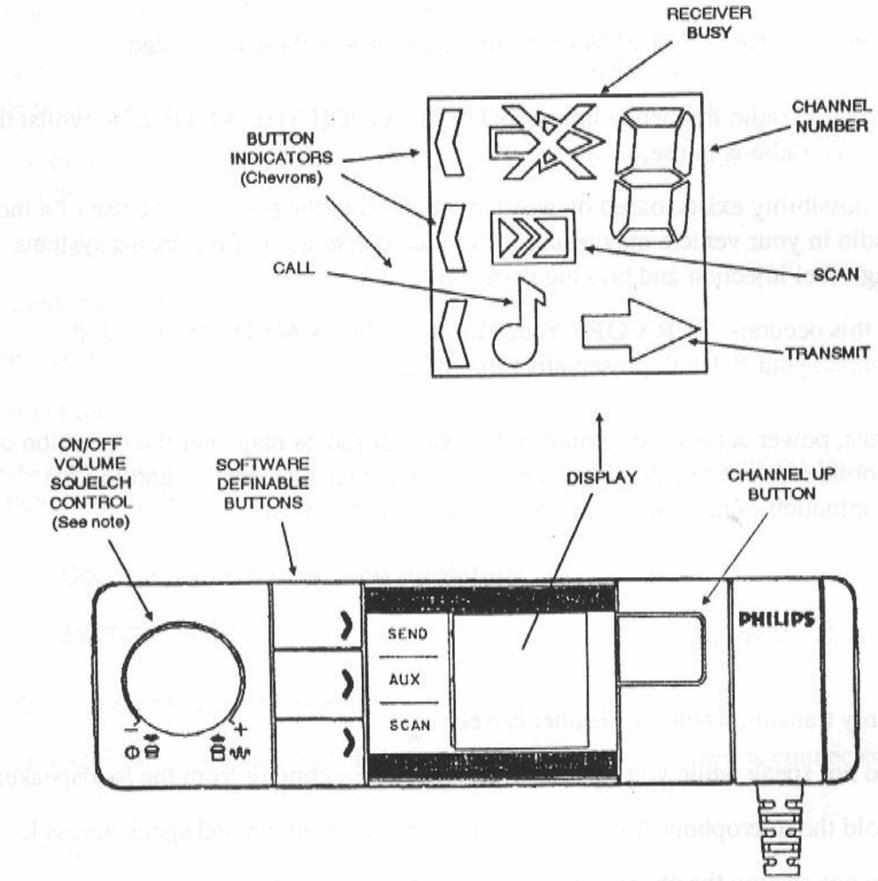
	1,2 Provisional	3 Channel Spacing (kHz)	4,5 Freq Band (MHz)	6 Freq. Stab	7 RF Power (Watts)	8 Control	9 Version	10 CTCSS Signalling	11 Sequent. Signalling	12 Installation	13 Mic.	14 Speaker	15 Noise Blanker	16 Equipment Label	17 Power Switch	18 Systems	19 Mute	20 Provisional
0								Not fitted.	Not fitted.	No kit.	Not required.	Not required.	Not fitted.	Philips.	Standard connection.	Not fitted.	Variable.	
1		S =12.5		5ppm -10 to +60°C.	1 to 25 (Std. VHF).	Local.	PRM8010.	ENC.	Selcall ENC	Swivel bracket	Standard.	Standard.	Fitted.	None fitted.	Bypassed for alarm.	Fitted.	Fixed.	
2		R = 20	E0 = 68 - 88	2.5ppm -10 to +60°C.	1 to 25 (Std. UHF).		PRM8020.	ENC/DEC.	Selcall ENC/DEC		Stick.	Compact.						
3		V = 25	B0 = 132 - 156	10ppm -10 to +60°C.	1 to 6 (Low UHF).			ENC/DEC plus 180° RTB.			DTMF.							
4		X = 30	A9 = 146 - 174	2.5ppm -30 to +60°C.	10 to 40 (High VHF).			ENC/DEC plus 120° RTB.										
5			TM = 400 - 440	5ppm -30 to +60°C.														
6			U0 = 440 - 470	10ppm -30 to +60°C.														
7			W1 = 470 - 500															
8			W4 = 500 - 520															
9																		

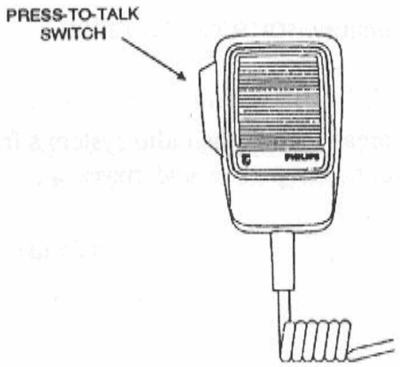
		1.2 Provisional	3 Channel	4,5 Freq Band	6 Freq. Stab	7 RF Power	8 Control	9 Version	10 CTCSS	11 Sequent.	12 Installation	13 Mic.	14 Speaker	15 Noise Blanke	16 Equipment	17 Power Switch	18 Systems	19 Mute	20 Provisional
									Not fitted.	Not fitted.	No kit.	Not require	Not require	Not fitted-	Philips.	Standard	Not fitted.	Variable.	
	7		S-12.5		5ppm	1 to 25	Local-	PRM8010.	ENC.	Selcall ENC	Swivel bracke	Standard-	Standard-	Fitted.	None fitted.	Bypassed	Fitted.	Fixed-	
	2		R - 20	E0 - 68-88	2.5pp-	1 to 25		PRM6020.	ENC/DEC.	Selcall ENC(		Stick.	Compact.						
	3		V - 25	80. 132-	1oppm	T T06			ENC/DEC			DTMF.							
	4		X - 30	A9 - 1445-	2.5ppm	10T040			ENC/DEC										
	6			TM-400-	5ppm														
	B			Lo - 440-	loppm														
	7			470-500															
	6			W4 500 -															
	9																		

1.5 OPERATING INSTRUCTIONS

These operating instructions have been extracted from the PRM8010 Operating Instructions.

PRM8010 9-CHANNEL CONTROL CONFIGURATION





NOTE

Push ON/Push OFF

Rotate for VOLUME

Pull and rotate for SQUELCH

1.5.1 Safety First

1. The use of the mobile radio while driving may be in breach of traffic regulations in some countries. Check with your local Traffic Authority for further details.

   Please do not use a hand-held microphone while you are driving.

2. DO NOT operate the mobile radio in an explosive atmosphere.

   Obey the "Turn Off TWo Way Radios" signs where these are posted.

3. To avoid radio frequency injury, DO NOT TOUCH THE ANTENNA whilst

   the mobile radio is in use.

4. A possibility exists, based on isolated incidents in the past, that the use of a mobile radio in your vehicle may result in the altered operation of electronic systems (eg. fuel injection and braking systems).

   If this occurs:- **TURN OFF** Your Mobile **Radio IMMEDIATELY,** and contact your Sales Representative for advice.

5. Fans, power accessories, window demisters or radios may alter the operation of your mobile radio. Consult the accessory manufacturer for details regarding the elimination of radio interference from such accessories.

1.5.2 Advice to User

1. Only transmit when the channel is free.
2. Do not speak while you can hear a tone sequence coming from the loudspeaker.
3. Hold the microphone 2 to 3 centimetres from your mouth and speak across it.
4. Do not occupy the channel any longer than is necessary.
5. Replace the microphone after use.
6. Identify yourself using your allocated radio identity.
7. Restrict the length of messages.
8. Avoid making calls from known poor signal areas such as the radio system's fringe areas or from screened areas, eg. an underground car park or underpass.

1.5.3 Introduction

The Type **PRM8010** transceiver is a versatile, microprocessor-controlled, dash-mounted, mobile radio designed to access facilities provided by the Private Mobile Radio Service.

The transceiver is software programmable to produce the options required to suit specific requirements. Though many options are available, each unit is dispatched from the factory programmed with a specific software application package, so that only a few parameters need to be varied in the field (eg. frequencies, selective call identities).

This guide describes all the facilities that are currently available, though some may not be available on your equipment.

The facilities that are available to you are most easily identified by examining the key label overlay on the front panel display.

Common functions and facilities are described in section 1.5.4.
Other functions are described in section 1.5.5.

Scanning functions are described in section 1.5.6.

Selcall functions are described in section 1.5.7.

Some specially adapted application packages may include facilities described separately in supplementary information sheets.

1.5.4 Common Functions And Facilities

1.5.4.1 SWITCH ON/OFF

To switch on, press the On/Off switch.

The LCD (Liquid Crystal Display) backlighting will be on when power is connected to the set.

To switch off, press the On/Off switch.

If the radio is wired for external on/off switching the On/Off switch will control only the display. The radio will be automatically switched on and off via external switching circuit.

1.5.4.2 SPEECH RECEPTION

Select the required channel by using 'Channel UP' button.

Pressing this button enables the selection of higher numbered channels, returning to the lowest channel number once the highest number has overflowed.

Set the 'squelch' control fully anti-clockwise.

In the absence of a signal the squelch control eliminates receiver noise and also suppresses weak interfering signals.

Adjust the 'volume' control until receiver noise is heard.

The volume control adjusts the speech level at the loudspeaker. Clockwise rotation increases the volume, anti-clockwise rotation decreases the volume.

Turn 'squelch' control clockwise just until the receiver noise disappears.

Note that this is the most sensitive setting of the squelch control. Turning the squelch control further clockwise will suppress weak interfering signals.

If the receiver is fitted with a 'fixed squelch' then the volume control is used as normal to obtain a suitable audio level when speech is being received.

If the radio is fitted with a 'squelch defeat' switch, this button may be used when operating in very weak signal areas.

1.5.4.3 SPEECH TRANSMISSION

To avoid interfering with other users of the operating channel, listen first to ensure that no transmissions are being made.

Make sure that the 'Busy' indicator is OFF.

Holding the microphone 2 to 3 centimetres from the lips, press the 'press-to-talk' switch (on the microphone) and note that the transmit indicator is turned ON. Speak clearly across the face of the microphone in a normal conversational manner.

Use the correct operating procedure, and keep transmissions short. Release 'press-to-talk' switch as soon as the message is finished and note that the transmit indicator is turned OFF.

When the 'transmit limit timer' option is fitted the transmitter will be turned off at the end of preset time, and a warning signal (if programmed) will be heard until the 'press-to-talk' switch is released. Re-pressing the 'press-to-talk' switch will turn on the transmitter.

If the 'transmit inhibit' option is fitted transmission will not be possible while a signal is being received, as indicated by the Busy Indicator.

1.5.5 Other Functions

This section deals with mobile facilities that are not apparent from the front panel of the transceiver, but which may significantly affect the operation of the transceiver.

These facilities are usually specially configured and require special operating practices which will be explained by your system controller or in supplementary information sheets. If you are unsure of how your equipment is configured with respect to these facilities you should contact your supplier.

1.5.5.1 TRANSMIT INHIBIT

If your equipment has the transmit inhibit facility programmed, you will be prohibited from transmitting either with the 'press-to-talk' switch or with any 'Send' button whenever the radio channel is busy and the 'Busy' indicator is on.

If the equipment is fitted with CTCSS and/or selective calling, the busy indicator and the transmit inhibit facility are both defeated whenever a valid call is received, so that you can respond to the call.

1.5.5.2 TRANSMIT LIMIT TIMER

The transmit limit timer limits the duration of the transmission. The transmission time may be set, in steps of one second, from 1 to 255 seconds. On expiry of the timer the transmission will cease and a continuous audible alarm will sound while the PTT switch is held pressed. To re-initiate the transmission the PTT switch must be released and then pressed.

1.5.5.3 TRANSMIT RE-PTT TIMER

The transmit re-PTT timer limits the minimum time between the release of the PTT switch, and the pressing of the PTT switch for the next transmission. The minimum time may be set, in steps of one second, from 1 to 255 seconds. If the switch is pressed during this time a continuous audible alarm will sound while the PTT switch is held pressed.

1.5.5.4 TRANSMITTER/RECEIVER LOCKOUT

These facilities are usually programmed together and only on carefully controlled 'closed' radio systems. On such systems users are prevented from listening to the channel.

1.5.5.5 CTCSS (CONTINUOUS TONE CONTROLLED SQUELCH SYSTEM)

When CTCSS encode only is fitted a sub-audio tone accompanies every mobile transmission. If the CTCSS decode is supplied, no communication will be heard unless the incoming transmission contains the correct CTCSS tone.

CTCSS decode can be bypassed by any of the following (if programmed):-

Removing the microphone from its cradle.

By enabling the monitor button.

1.5.5.6 MICROPHONE CRADLE OPERATION

Depending of the options programmed, the cradle can affect the operation of the transceiver in any of the following ways:

Mobile may transmit Automatic Number identification whenever the microphone is removed from its cradle.

Mobile may enter Monitor mode whenever the microphone is removed from its cradle. Calls may be reset whenever the microphone is returned to its cradle.

Scanning will only be active if the microphone is in its cradle.

If the microphone is removed from its cradle while the scan has stopped on a channel, that channel will remain selected until the microphone is returned to its cradle.

If the microphone is removed from its cradle while the transceiver is still scanning, the priority channel will be selected. The channel display will

1.5.6 Scanning Functions

When fitted this option allows a mobile to scan a number of radio channels for a valid signal. There can be up to 9 channels in a scan group and one of these can be designated as a Priority channel. This channel will differ from the basic channels in the following:

If there is a priority channel programmed, the radio will check the priority channel for the presence of a signal in between normal channels.

If the microphone is removed from its cradle while the transceiver is still scanning, the priority channel will be selected and the Channel Display will

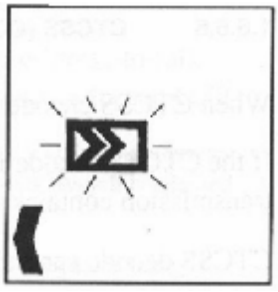
While on a scan channel, mobile will still check the priority channel for the presence of a valid signal until the microphone is removed from its cradle.

Scanning will only be active if the microphone is in its cradle (ie. on-hook)

1.5.6.1 OPERATION

To enter Scan mode press the SCAN button

The Scan chevron will turn ON. The Channel display will be blanked and the SCAN indicator will start flashing.



If the error tones sound when the SCAN button is pressed, it will mean that:

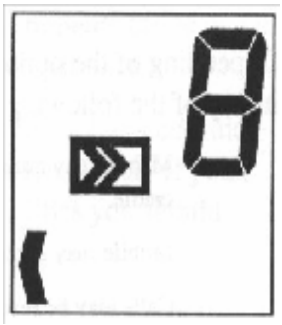
the scan group is empty, or

the current channel is not allowed as a priority priority channel, or

the 'press-to-talk' switch is currently pressed.

The radio will scan the selected channels in sequence. The scan will continue until a valid signal is found.

When a valid signal is found the mobile will halt scanning, the 'Scan' indicator will cease flashing to become steady, and the channel display will show the channel number selected. .



Remove the microphone from its cradle.

This channel will remain selected until the microphone is returned to its cradle and scanning resumes.

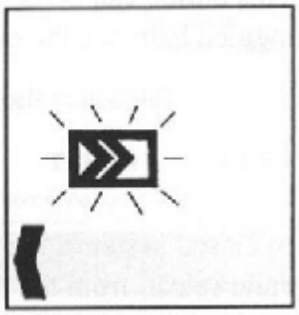
Terminate the scan mode by pressing the 'Scan' button.

The mobile will return to the channel that was selected before the scan function was initiated.

1.5.6.2 SELECTION OF PRIORITY CHANNEL (if enabled)

Select the required channel by using 'Channel UP' button.

Use the 'SCAN' button to initiate scanning.



The channel selected will automatically become the priority channel.
Note: The 'ERROR TONE' will sound if the channel that is selected is not permitted as a scan channel.

1.5.7 Selective Call Facilities

Selective call is an optional fitting which can allow the mobile radio to respond to, and/or initiate a signal carrying an identifying number.

A number of different operations are available depending on the system configuration and the features programmed.

The facilities currently available are indicated below. Please note that some of these may not be available on your equipment.

1.5.7.1 SEND 1

The Send button causes a programmed identity to be transmitted. This identity is used to identify the mobile to the base control.

1.5.7.2 SEND 2

Used as Send 1 but provides for a second identity.

1.5.7.3 ALARM

Alarm is a special version of Send. It is used to indicate the presence of an alarm condition or it can be used as a priority call request. The exact use of this function will depend upon how your particular radio system has been designed. You should have specific instructions about when this button is to be used.

Please note that the mobile radio is controlled by the base controller during the emergency mode.
Alarm may also be activated by a special switch (if fitted),external to the equipment.
Alarm condition can be reset from base control, or by disconnecting the radio from the battery.

1.5.7.4 EXTERNAL ALERT

This button is used to control an external device, such as the vehicle horn. It is normally switched on when you expect to be outside your vehicle and it will be activated, whenever your equipment receives a valid call.

1.5.7.5 MONITOR / RESET

This button can be programmed to enable you to listen to all calls on the channel. It can be toggled between the quiet and listen modes.

This button also cancels the called indicator.

1.5.7.6 RESET

In closed systems, the mobile is allowed to listen to a voice channel only when it receives a valid selcall from the base control. The Reset button allows the mobile to revert to quiet mode. When used it cancels the called indicator.

1.5.7.7 TRANSPOND

Transpond provides a facility for the mobile to automatically transmit a predefined identity to acknowledge that a call has been received. This switch is used to enable/disable this facility.

1.5.7.8 SELCALL RECEPTION

Whenever a valid call is received the equipment will display the 'Call' indicator. It will also sound the appropriate call alert.

You may answer the call by operating the 'press-to-talk' switch. The indicator and alert tone will be cancelled. Additionally, if programmed, removing the microphone from its cradle will cancel the indicator and alert tone. Alternatively the call may be cancelled by pressing the monitor button once.

If you do not answer the call, the call alert will stop after a few seconds but the indicator will remain on. Depending on how your radio system is configured, the call can be terminated in one of the following ways:

Removing the microphone from its cradle.

Pressing the 'Monitor' button once.

By receipt of 'Remote Reset' signal from the base

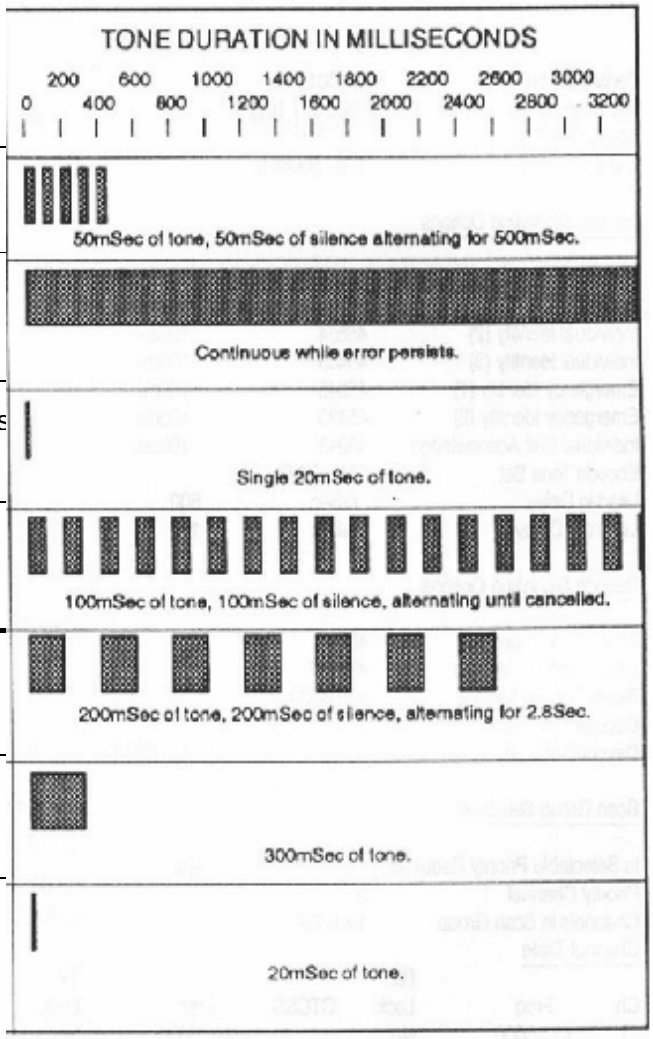
control. By expiry of the 'timed reset timer'.

By returning the microphone to its cradle.

1.5.8 Alert Tones

The frequency of all 'alert tones' is 500Hz.

TYPE OF ALERT	
ERROR TONE	Generated when operator presses an invalid button.
2 CONTINUO TONE ERROR	Generated on Invalid of PTT, or If microphone left of cradle
3 KEY BEEP TONE	Generated when any button Is pressed
4 DECODE 1 ALERT TONE	Generated for selcall decode response.
URGENT ALERT TONE	Generated for selcall urgent response.
6 GROUP ALERT TONE	Generated for selcall group response.
NORMAL DECODE ALERT TONE	Generated for selcall normal response.


TONE DURATION IN MILLISECONDS
200 600 1000 1400 1800 2200 2600 3000
0 400 800 1200 1600 2000 2400 2800 3200
50mSec of tone, 50mSec of silence alternating for 500mSec.
Continuous while error persists.
Single 20mSec of tone.
100mSec of tone, 100mSec of silence, alternating until cancelled.
200mSec of tone, 200mSec of silence, alternating for 2.8Sec.
300mSec of tone.
20mSec of tone.

1.5.9 Equipment Data Sheet

An individual data sheet listing all transmitter and receiver frequencies, including signalling information, is supplied with each transceiver. It is important that this data sheet is retained for future use such as the equipment requiring repair or change to parameters (eg. channels or identities). A sample data sheet is shown below.

Serial Number	200001	
Hardware 12NC	9525 001 10072	
Application Code		
Frequency Band	470 - 500MHz	
<u>Encode Signalling</u>		
Options		
Encode Type	Identity	Tone Period
Individual Identity (1)	53454	l00ms
Individual Identity (2)	45554	l00ms
Individual Identity (3)	45453	l00ms
Emergency Identity	45345	l00ms
Emergency Identity	45435	looms
Individual Call	45345	looms
Encode Tone Set	CML CCIR	
Lead in Delay	mSec	600
Lead out Delay	msec	100
<u>Decode Signalling</u>		
Options		
Indiv Decode Identity	45345	
Group Decode	435345	
Reset Decode Identity	43534534	
Decode Tone Period		l00ms
Decode Tone Set		CIVIL CCIR
<u>Scan Group Selection</u>		
Is Selectable Priority Required		No
Priority Channel	3	
Channels in Scan	14679	

Channel Table

Ch	Freq	Rx Lock	CTCSS	Freq	TX Lock	CTC/ Selc	Co	Scan	Power
1	471.0000	No		471.0000	No	Yes	No	Yes	High
3	475.0000	No				No	No	Yes	High
4	476.0000	Yes				No	No	Yes	High
5	477.0000	No		478.0000	Yes	Yes	No	No	High
7	480.0000	No		481.0000	No	No	No	Yes	High
9	495.0000	No				No	Yes	Yes	High

SECTION 2 TECHNICAL SPECIFICATIONS

Unless otherwise stated, specifications apply for an ambient temperature of 25 Deg C and 13.8V supply.

2.1 GENERAL

Operation

Single- or two-frequency simplex.

Modulation

Frequency.

Supply Voltage

10.8V to 16.2V dc, negative earthed to chassis.

Frequency Bands

VHF	UHF
E0 68 - 88 MHz	Tm 400 - 440 MHz
B0 132 - 156 MHz	U0 440 - 470 MHz
A9 146 - 174 MHz	W 1 470 - 500 MHz
	W4 500 - 520 MHz

Channel Spacing

VHF	UHF
12.5 kHz	12.5 kHz
20 kHz	20 kHz
25/30 kHz	25 kHz

Frequency Stability

UHF & VHF (option) crystal).	+/-5ppm	-10 Deg C	to	+60 Deg C (better quality
VHF crystal).	+/-10ppm	-10 Deg C	to	+60 Deg C (standard
VHF & UHF (USA) option).	+/-5ppm	-30 Deg C	to	+60 Deg C (extended temp
UHF	+/-2.5ppm	-10 Deg C	to	+60 Deg C (TCXO).
UHF	+/-2.5ppm	-30 Deg C	to	+60 Deg C (TCXO).
VHF option)	+/-10ppm	-30 Deg C	to	+60 Deg C (extended temp

Switching Bandwidth

Frequency band coverage without retuning

UHF TM 40MHz, U0 30MHz, W 1 30MHz, W4 20MHz
VHF A9/B0 band 30MHz
VHF E0 band 20MHz

Channel Capacity

i) 9-channel

ii) 64-channel Current Consumption

	VHF	UHF
Off state	less than 10mA	less than 350mA
Rx standby (no AF output)	less than 10mA	less than 350mA
Tx (25W)	less than 5.5A	less than 6.5A

Type Approval Compliance

The PMR80 is designed to comply with the following regulatory specification standards.

i)	Australian DOC	RB206, RB207, RB234B
ii)	New Zealand	RTA25
III)	Canada	RS119
iv)	European	CEPT TR24-01 Annex 1,2,5,7 MPT 1306, MPT 1316, MPT 1326.
v)	EIA	RS 15213, RS204C. (Does not comply with squelch sensitivity 17.0, or Temp range 22.0).
vi)	FTZ	A446 82023, AA446 82024.

Dimensions

Length; 203mm (210mm including Volume knob). 160mm.
Width; 160mm.
Height; 45mm.
Weight; less than 1.4kg (including cradle).

2.2 RECEIVER

Sensitivity

12dB sinad for less than 0.31uV pd. at the antenna socket, for 1 kHz at 60% maximum deviation and 50% rated AF output power.

Adjacent Channel Selectivity

i). DOC method
VHF Greater than 4.1mV pd (73dB wrt 0.31uV).
UHF Greater than 5 mV pd (74dB wrt 0.31uV).

Intermodulation Rejection Ratio

Three generator method, greater than 75dB at 100200kHz above and below carrier to avoid selectivity limitations.

Spurious Response Rejection Ratio

i) VHF Greater than 85dB with a single signal.

ii) UHF Greater than 80dB with a single signal.

Blocking

Greater than 93dB ratio at 150kHz offset, 2-generator method.

Modulation Acceptance Bandwidth

i) 12.5 kHz channel spacing, greater than +/-4kHz.
ii) 20 kHz channel spacing, greater than +/-7.0kHz.
iii) 25/30kHz channel spacing, greater than +/-8.5kHz.

Spurious Radiation

9kHz to 1GHz less than 2 nW.
1GHz to 4GHz less than 20 nW.

AF Regulation

Less than 1dB variation in AF level for RF input level change from 0.3uV to 100mV PD.

Residual Hum and Noise

channel spacing	12.5kHz	25/30kHz
VHF	41dB	47dB
UHF	40dB	46dB

Reference 1 kHz at 60% deviation. 1 mV RF level. CCITT weighted. CTCSS not fitted.

Audio Frequency Response

Measured at the loud speaker for a constant deviation at 20% of maximum.
Within +l dB to -3dB of -6dB per octave de-emphasis relative to 1 kHz over 300Hz to 3000Hz, CTCSS not fitted.
With CTCSS fitted within +1.5 to -3dB.

Audio Output

i) 4 watts into 4 ohms, less than 10% THD with 1kHz at 60% maximum deviation.
ii) 16 watts into 4 ohms, optional.

Audio Distortion

Less than 5% THD for 300mW into 4 ohms, 1kHz at 60% deviation.

Mute Response Time

Mute set to open at 20dB SINAD.
Response for 1 uV RF level; less than 40mSec.

Mute Range

Channel Spacing	12.5kHz	25kHz
maximum	18 to 20dB	20 to 25dB SINAD.
Minimum	l0dB	l0dB SINAD.

2.3 TRANSMITTER

Power Output

Adjustable; 1 to 6 watt, 1 to 25 watt, 10 to 40 watt.

Spurious Emission

Less than 0.25uW 100kHz to 1GHz, less than 1uW 1GHz to 4GHz.

Residual Hum and Noise

Greater than 40dB (Reference 1 kHz at 60% deviation. DC to 25kHz bandwidth CCITT weighted and 6dB/octave de-emphasis).

Microphone Sensitivity

Less than 20mV rms at 1 kHz to achieve 60% maximum deviation. Standard sensitivity setting, 40mV +/-10%; Optional setting, 5mV

Audio Distortion

Less than 3%. Reference 1kHz at 60% deviation.

Audio Frequency Response

i) 25kHz Channel Spacing.
Within +1 to -3dB of a +6dB per octave pre-emphasis, over 300 to 3000Hz (without CTCSS).
With CTCSS, within +1.5 to -3dB.

ii) 12.5kHz Channel Spacing.
Within +1 to -3dB over 300 to 2550Hz (without CTCSS).
Within +1.5 to -3dB over 300 to 2550Hz (with CTCSS).

Transmitter Rise Time

Less than 40mSec from operation of the PTT to achieve 70% of output power.

2.4 SIGNALLING

2.4.1 PRM80 Selcall Specification

2.4.1.1 ENCODER

(i) Tone Deviation.
Factory preset to 80% or system deviation adjustment range typically 33% to over 100% of system deviation.

(ii) Tone Distortion.
Not greater than 10% at TX VCO input.

(iii) Tone Frequency Range.
63 possible tones in the range 459Hz to 2937Hz. See Table 2.2 for details.

(iv) Tone Amplitude Variation.
Not greater than 6dB over 459Hz to 2937Hz.

(v) Tone Frequency Error.
Not greater than 1.0% -30C to +60C.

(vi) Tone Period.
14 possible durations from 20 to 255mSec. Accuracy greater than 3.0%. The required tone period may be selected from the following:

a)	20 mSec.	b)	33 mSec.
c)	40 mSec.	d)	60 mSec.
e)	70 mSec.	f)	80 mSec.
g)	100 mSec.	h)	120 mSec.
i)	140 mSec.	j)	150 mSec.
k)	200 mSec.	1)	210 mSec.
m)	250 mSec.	n)	255 mSec.

(vii) Lead-in-Delay.
0 to 65Sec. Accuracy greater than 1%.

(viii) Lead-out-Delay.
0 to 255mSec. Accuracy greater than +0, -1 mSec.
(ix)Send Repeat Rate.
Approx 100mSec following end of transmission. Additional send keystrokes are ignored during encode.
(x)Code Formats.
Up to 10 tones per sequence.

2.4.1.2 Decoder

(i) Sinad Sensitivity.
For 90% decode success rate sinad is measured at speaker output.

1. Standard Selcall.

20mSec	14dB Sinad
40mSec	15dB Sinad
l00msec	13dB Sinad
255mSec	l4dB Sinad

2 Enhanced Selcall.
20mSec TBA
40mSec TBA
100mSec TBA
255mSec TBA

(ii) Deviation Sensitivity.
Minimum deviation for 90% success rate and full receiver quieting.

1 Standard selcall.
Less than 0.3kHz deviation.

2. Enhanced selcall.
TBA.

(iii) Decode Bandwidth.
80% deviation and full quieting.

CCIR	1.5% to 3 %
ZVEI	2.0% to 4.5%
EEA	1.5 % to 3.5 %
EIA	1.5 % to 3.5 %
DZVEI	2.0% to 4.5%
NATEL	1.3% to 1.7%

(iv) Valid Tone Period for Successful Decode.
80% deviation and full quieting.

-40% to +70%

(v) Code Format.
A successful decode will occur if the correct code address is preceded with and/or followed by erroneous tones or noise.

(vi) Decode Recognition.
Upon receipt of correct decode address, no action occurs (ie mute open, auto acknowledge, etc) until approximately one tone period has elapsed.

2.4.2 PRM80 CTCSS Specification

2.4.2.1 Encoder

(i) Tone Deviation.

25kHz channel spacing	500 to 700Hz.
20kHz channel spacing	400 to 560Hz.
12.5kHz channel spacing	250 to 350Hz.

7% to 36% of systems deviation adjustment range.

(ii) Tone Distortion.
Less than 5.0%.

(iii) Frequency Accuracy.
+/- 0.30% over -30 degC to +60 degC.

(iv) Number of Tones.
There are, including disabled, 38 available tones. See Table 2.1.

2.4.2.2 Reverse Tone Burst.

In order to prevent the mute "tail" associated with the de-response time of CTCSS decoders, the mobile may be equipped with reverse tone burst (RTB). This RTB, occurs at the end of CTCSS transmission and consists of a period of CTCSS tone of either 180 or -120 degrees phase difference to that previously sent. The period of this tone is dependent on the tone frequency, see Table 2.1.

The RTB installation may be either hardware or software.

(i) Hardware RTB.

RTB phase Shift:	120 degrees +/- 10 degrees, lagging.
RTB duration:	Between 80mSec to 150mSec. CTCSS tone frequency dependent. See Table 2.1.
RTB Amplitude Variation (across CTCSS tone set).	+/- 2dB.

(ii) Software RTB.

RTB phase shift:	180 degrees +/- 10 degrees, lagging.
RTB duration:	between 80mSec to 150mSec. CTCSS tone frequency dependent. See Table 2.1
RTB amplitude variation (across CTCSS tone set).	0.5dB.

2.4.2.3 Decoder

(i) Tone-Set.
as per Encoder.

(ii) Bandwidth.
+/- 3.0% max.

(iii) Deviation Sensitivity.
Better than 6% of system deviation (for decode with full RF quieting).

(iv) Noise Immunity.
Less than 500mSec dropout per minute for l0dB sinad
(CTCSS tone deviation 10% of system and sinad signal of 60% deviation at 1kHz).

(v) False Decode Rate.
Less than 5 false decodes per minute (no carrier input).

(vi) Talkoff.
I nterfering tone deviation for loss of decode (CTCSS tone deviation 10% of system).

Full quieting RF signal:	310Hz to 3kHz 90% of system deviation (for no dropouts).
20dB sinad RF signal:	320Hz to 3kHz ; 90% of system deviation (for no dropouts in one minute).
12dB sinad RF signal:	350Hz to 3kHz; 90% of system deviation (for no dropouts in one minute).

(vii)	Response Time;	Less than 250mSec. (With a full quieting signal of 67Hz at 10% of system deviation; 67Hz gives the slowest times).
(viii)	De-response time;	Less than 250mSec.

2.4.2.4 Speech Rejection Filter

(i) Response.
300 Hz 0 dB.
250 Hz <-36 dB.

Table 2.1 CTCSS Tonesets Available In the PRM80

FREQ. (Hz)	Tone Number	R.T.B. Duration (mSec)
(disabled)	00	----
67.0Hz	17	150
71.9 Hz	18	140
74.4 Hz	19	140
77.0 Hz	20	140
79.7 Hz	21	130
82.5 Hz	09	130
85.4 Hz	22	130
88.5 Hz	01	130
91.5 Hz	23	120
94.8 Hz	10	120
97.4 Hz	38	120
100.0 Hz	02	120
103.5 Hz	11	120
107.2 Hz	03	110
110.9 Hz	12	110
114.8 Hz	04	110
118.8 Hz	13	110
123.0 Hz	05	110
127.3 Hz	14	110
131.8 Hz	06	110
136.5 Hz	15	110
141.3 Hz	07	110
146.2 Hz	16	110
151.4 Hz	08	110
156.7 Hz	24	110
162.2 Hz	25	90
167.9 Hz	26	90
173.8 Hz	27	90
179.9 Hz	28	90
186.2 Hz	29	90
192.8 Hz	30	90
203.5 Hz	31	90
210.7 Hz	32	80
218.1 Hz	33	80
225.7 Hz	34	80
233.6 Hz	35	80
241.8 Hz	36	80
250.3 Hz	37	80

TABLE 2.2 Selcall Tonesets Available In the PRM80

TONE #	Manucturer s Type N	CML	ST-500	SIG TEC	SIG TEC	SEPAC	CML	ST-500 0	SIG TEC
	International System No.-	CCIR	CCIR	CCIR	CCIRH	CCIR	EEA	EEA	EEA
0		1981	1981	1981	1981	1981	1981	1981	1981
1		1124	1124	1124	1124	1124	1124	1124	1124
2		1197	1197	1197	1197	1197	1197	1197	1197
3		1275	1275	1275	1275	1275	1275	1275	1275
4		1358	1358	1358	1358	1358	1358	1358	1358
5		1448	1446	1446	1448	1448	1448	1446	1446
6		1540	1540	1540	1560	1540	1540	1540	1540
7	.	1640	1640	1640	1640	1640	1640	1640	1640
8		1747	1747	1747	1747	1747	1747	1747	1747
9		1860	1860	1860	1860	1860	1860	1860	1860
A		2400	-------	2110	2400	2400	1055	1055	2110
B		930	1055	2400	930	1055	930	-------	1055
C		2247	2400	1055	2247	2247	2247	2400	2400
D		991	-------	2247	991	991	991	-------	2247
E		2110	2110	930	2110	2110	2110	2110	930
F		------	-------	991	1055	-----	-----	-------	991
TONE #	**Manufacturer's Type No.-**	SEPAC	CML	ST-500	'SIGTEC	SEPAC	SIGTEC	SEPAC	SIGTEC
	Intematonal System No.	EEA	ZVEI	ZVEI	ZVEI-1	ZVEI-1	ZVEI-2	ZVEI-2	ZVEI-3
0		1981	2400	2400	2400	2400	2400	2400	2200
1		1124	1060	1060	!1060	1060	1080	1060	970
2		1197	1160	1160	1160	1160	1160	1160	1060
3		1275	1270	1270	1270	1270	1270	1270	1160
4		1358	1400	1400	1400	1400	1400	1400	1270
5		1446	1530	1530	1530	1530	1530	1530	1400
6		1540	1670	1670	1870	1670	1670	1670	1530
7		1640	1830	1830	11830	1830	1830	1830	1670
8		1747	2000	2000	2000	2000	2000	2000	1830
9		1880	2200	2200	2200	2200	2200	2200	2000
A		1055	2800	970	2900	2800	970	885	2400
B		970	810	-------	2800	970	885	741	885
C		2247	970	2800	741	885	741	2600	741
D		2400	886	-------	970	--------	2600	-------	2600
E		2110	2600	2600	810	2600	2800	970	2800
F		-------	------|	-------	886	--------	600	-------	600
TONE #	**Manufacture's Type No. -+**	SEPAC \CML	ST-500 \CML	ST-500	ST-500	SIGTEC	SIGTEC	SEPAC	ST-500
	Intemadonal I System No.	ZVEI-3	ZVEI-3	DZVEI	DZVEI	NATEL	EIA	EIA	EIA
0		2200	2400	j2200	2200	1633	600	600	600
1		970	1060	970	970	631	741	741	741
2		1060	1160	1080	1060	697	882	882	882
3		1160	1270	1180	1160	770	1023	1023	1023
4		1270	1400	1270	1270	852	1164	1164	1164
5		1400	1530	1400	1400	941	1305	1305	1305
8		1530	1870	1530	1530	1040	1446	1446	1446
7		1670	1830	1670	1670	1209	1587	1587	1587
8		1830	2000	1830	1830	1336	1728	1728	1728
9		2000	2200	2000	2000	1477	1869	1869	1869
A		885	885	2600	825	1805	459	2151	2151
B		741	-------	-------	-------	1995	2151	1091	-------
C		2600	810	886	2600	1300	2600	2400	2010
D		-------	-------	810	-------	1700	2010	-------	-------
E		2400	970	2400	2400	2175	2433	459	459
F		--------	--------	-------	-------	2937	2292	-------	--------

SECTION 3 TECHNICAL DESCRIPTION

3.1 GENERAL OVERVIEW

Shown in figure 3.1 is the overall simplified block diagram of the PRM80.

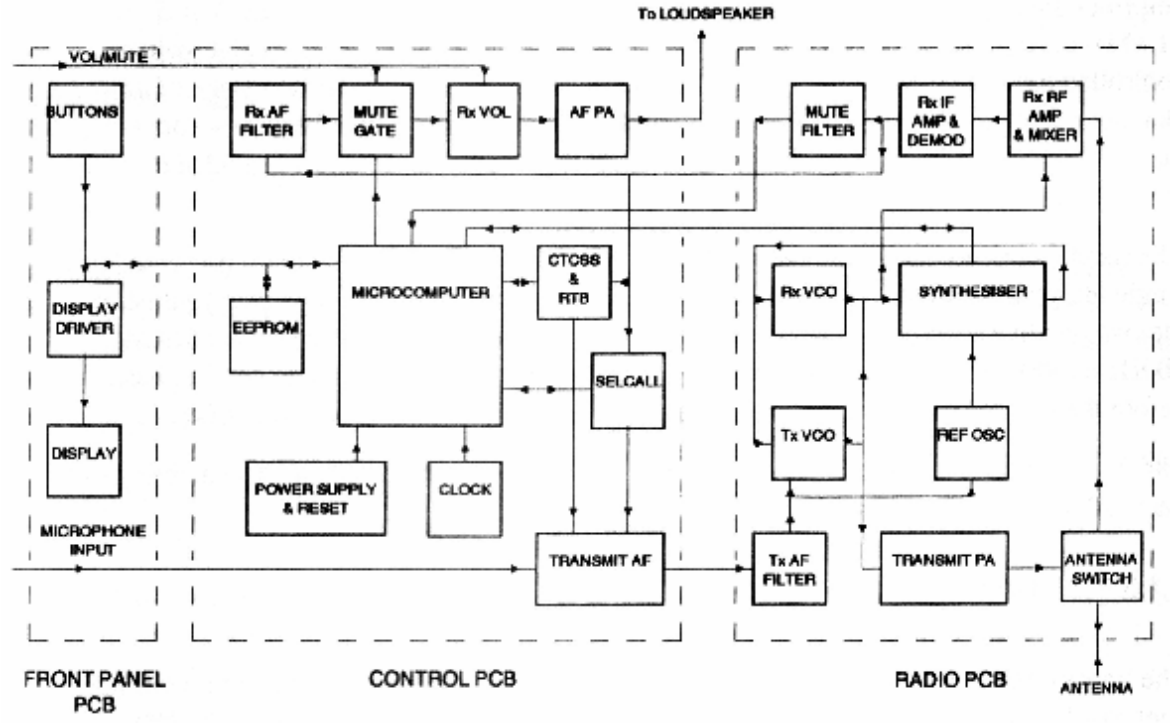


Figure 3.1 PRM80 - Overall Block Diagram

The transceiver consists of three printed circuit board assemblies.

i) Front Panel Board

Containing the liquid crystal display, its driving circuit, push button switches and display backlighting.

ii) Control Board

Containing the microprocessor with its associated clock and latches, EEPROM memory, power supply and reset circuit, transmitter audio processing, receiver audio processing, selective call audio processing and CTCSS signalling option.

iii) Radio Board

Containing the transmitter power amplifier with antenna switch, receiver front end filters and mixer, receiver IF and demodulator, synthesizer and reference oscillator, transmit and receive voltage controlled oscillators, and transmitter audio low pass filter. All the frequency band and channel spacing related components are on this board assembly.

3.1.1 Receiver

The receiver concept utilizes a double conversion superhetrodyne principle with first and second intermediate frequencies of 21.4 MHz and 455kHz respectively.

The front end of the receiver uses electronically tuned bandpass filters and a radio frequency amplifier ahead of a double balanced mixer. The frequency conversion to the first IF of 21.4MHz occurs in this mixer with the local oscillator injection from the receive voltage controlled oscillator. Monolithic crystal filters at 21.4MHz provide the first stage of adjacent channel rejection. Amplification at 21 4MHz is provided ahead of the frequency conversion to the second IF of 455kHz. The final stage of adjacent channel rejection is provided by a ceramic filter.

The second conversion, IF limiter amplification and FM demodulation are all processed in a single integrated circuit. The demodulated audio out of this IC is first low pass filtered to remove residual 455kHz products and then further audio frequency processing, such as 300Hz to 3000Hz band pass filter and de-emphasis, is provided. The mute gate is placed before the volume control adjustment, which is ahead of the audio power amplifier.

The demodulated output is also high pass filtered, amplified and detected. The quieting of the detected noise provides for mute control.

3.1.2 Transmitter

The transmitter power amplifier line up, amplifies the signal output of the transmit voltage controlled oscillator, which is at the final carrier frequency. The amplification is sufficient to achieve 25 watts final output from the nominal 20 milliwatt level of the VCO.

The amplifier design is broadband without mechanical tuning. Power output is stabilized by the action of a feedback loop. This power control loop circuit also protects the amplifier from excessive load mismatch conditions and temperature rise. The output from the amplifier is coupled to the antenna socket via the antenna change over switch and the harmonic rejection low pass filter.

Power output may be set between 1 watt and 25 watts, with the option of switching between two preset power levels. An RF output detector is monitored so that in the presence of RF power the transmit indicator is illuminated.
Transmit audio processing begins with an active microphone containing a transistor pre-amplifier. In the transceiver unit the microphone signal is filtered and amplified, ahead of

an amplitude limiter stage. Following the limiter the signal is low pass filtered prior to modulating the transmit VCO. Provision is made to combine microphone and signalling audio.

3.1.3 Synthesizer

The frequency synthesizer provides the functions of excitation for the transmitter power amplifier, and the receiver first local oscillator. A single phase locked loop principle is used with synthesis at the required final frequency. The phase locked loop comprises the transmit and receive VCOs, a prescaler/divider, programmable divider and phase comparator, reference oscillator,and loop low pass filter. The action of the loop is to phase lock the VCO frequency to the stable reference frequency which is derived from a crystal oscillator.

The synthesizer is reprogrammed to a new frequency by a serial sequence of data commands to the programmable divider IC, this data is latched in the IC. For frequency modulation in transmit mode, both the transmit VCO and the synthesizer reference oscillator have modulation applied.

3.1.4 Microprocessor Control

A single chip 8-bit CMOS microprocessor forms the basis of the computer control circuitry. Within this device is a masked program read only memory. This program performs the generation and detection of selective call tone sequential signalling, as well as the operational characteristics of the selcall system response. In addition to this, other major functions include programming of the synthesizer, controlling the display of LCD information, controlling the receiver audio mute and transmit microphone mute, monitoring the front panel buttons,controlling CTCSS and reverse tone burst signalling, and performing the task of programming and reading the electrically erasable memory.

The electrically erasable memory contains the user customizable information, which includes features such as channel frequency, signalling system requirement (toneset, code, system response etc.), transmit limit timer value. This memory is programmed or read via the microprocessor, from the microphone socket interface.

The microprocessor operates from an external 1'6MHz clock using a crystal oscillator. This clock frequency is divided by an additional IC to provide a clock signal of 1 MHz for the CTCSS option.

A latch is provided between the microprocessor and several controlled functions of the radio transceiver. This latch provides a port expansion of the microprocessor and isolates some of the more sensitive radio control interfaces from the microprocessor clock noise.

3.1.5 Signalling

Selective call tone frequency generation is performed in the microprocessor. A digital to analog convertor provides a low distortion encode signal. Receiver demodulated selcall is bandpass filtered before a zero-crossing detector. This circuit produces impulses at twice the frequency of the demodulated selcall tones and provides a waveform suitable for processing directly by the microprocessor.

The CTCSS encode and decode function is performed in a single integrated circuit. The IC is controlled by the microprocessor. The encoder/decoder IC also provides a high pass filter when in receive mode to remove the demodulated tone ahead of the audio power amplifier, and in transmit mode to reject low frequency microphone audio prior to modulating the transmit VCO.

A reverse tone burst feature is provided in two formats. A 180 degree phase shift is available in encode directly out of the encoder/decoder IC and a -120 degree phase
shift is provided by an additional circuit.

3.1.6 Power Supply and Reset

Three regulated supply voltages are required for operation of the transceiver circuitry. These are +9volt, +5volt and +23volt. The +9volt and +5volt regulated supplies are derived from integrated circuits and the +23volt supply is generated by a multivibrator circuit and a voltage multiplier. This high voltage supply is used to provide a wider control voltage range for the varicap diodes used in the VCOs and receiver front end filters.

A permanent +5volt trickle supply is provided for the microprocessor. This maintains stored information during short duration power failures and also retains the last programmed state when the transceiver is switched off.

To ensure reliable operation of the microprocessor, an interrupt and reset circuit is provided. This circuit detects power failure and induces the microprocessor to prepare for a reset. The timing between interrupt and reset is carefully controlled to ensure that the microprocessor is enabled and disabled in a predictable manner during supply failure and restoration. The reset operation is also rate limited and will prevent the enabling of the microprocessor before the supply voltage has sufficiently stabilised. The interrupt and reset operation is designed to detect total loss of primary power, or supply voltage reduction below the regulator limit of the +9 volt regulator.

3.1.7 Controls and Display

In both the 9-channel and 64-channel versions of the front panel,the visual display indicators are provided by a liquid crystal display. A single integrated circuit is used to drive the display. Information to be displayed is programmed and latched into the driver IC by the microprocessor.

The momentary-acting push-button switches are connected directly to a set of dedicated inputs on the microprocessor.

3.2 DETAILED TECHNICAL DESCRIPTION

3.2.1 Receiver

3.2.1.1 GENERAL

The double conversion receiver design is intended for narrow band frequency modulation systems only. Figure 3.2 shows the simplified block diagram of the receiver excluding the final stages of audio processing.

3.2.1.2 FRONT END

3.2.1.2.1 UHF Section

The UHF front end filter utilizes five ceramic coaxial resonators which are effectively quarter-wave transmission lines with one end short circuited to ground. A bandpass filter is formed by capacitively coupling two resonators together, and varicap diodes are used to electronically tune the resonant frequency of the filter. Referring to the circuit diagram, X400 and X401 are the resonators in the first input filter pair, and D400 to D407 are the varicap tuning diodes.

Capacitors C403, C404 and C405 form the main signal coupling path for the filter when tuned to the high frequency end of the required band. Conversely, capacitors C402, C406 and C408 sustain coupling at the low frequency end. This technique helps maintain a constant filter insertion loss and bandwidth over the tuning range. The tuning of the varicap diodes is effected by a control voltage coupled from the synthesizer via resistors R401 and R403.

The remainder of the front end consists of a low noise transistor preamplifier in TR400, followed by a tuned bandpass filter using three coupled resonators, X402, X403 and X404. This three-section filter operates in a similar manner to the first pair already described. Conversion to the first IF frequency of 21.4MHz is achieved with the double balanced ring diode mixer U400.

3.2.1.2.2 VHF Section

The VHF front end filter is realized by two pairs of coupled helical resonators. The first input bandpass filter FL400 comprises two helical resonators which are arranged in an inter-digital configuration. This is achieved by grounding the opposite ends of each coil and reversing the winding direction of one coil.

The coils are mounted horizontally on the printed circuit board and are positioned in such a manner as to achieve mutual coupling. A tin-plated brass shield is placed over the top of the coil pair. Each coil is mechanically fine tuned with a copper tuning core.

Varicap diodes D400 to D407 are placed across the coils for electronic tuning. Resistors R400 to R403, and R413 couple the do bias voltage from the synthesizer to control the tuning.

The remainder of the VHF front end consists of a low noise transistor preamplifier in TR400, followed by a second pair of helical interdigital bandpass filters FL401. The four coils

required for the total front end filtering are mechanically pre-aligned by the tuning cores, but once set require no further readjustment.
Conversion to the first IF frequency of 21.4MHz is achieved with the double balanced ring diode mixer U400.

3.2.1.3 IF SECTION

Following the double balanced mixer module U400, an IF pre-amplifier, TR401, provides additional IF gain and also presents a suitable impedance match to the crystal filter FL403. Further IF amplification is provided at 21.4MHz by TR402, and this stage is also designed to load the crystal filter with an optimum load impedance. Approximately 30dB of overall gain is provided at 21.4MHz ahead of the second IF conversion.

IC400 contains the receiver second mixer and second local oscillator, limiter amplifiers operating at the second IF frequency of 455kHz, and the FM de-modulator.

The 21.4MHz signal is connected to the input of the second mixer at PIN 16 of IC400. The second local oscillator has its active components internal to IC400 with the crystal reference, XL400, connected externally at PIN 1.

The output of this second mixer appears at PIN 3, and here the second IF difference frequency of 455kHz is filtered by a ceramic filter, FL404. This filter provides the final stage of adjacent channel rejection, and it's performance in conjunction with FL403 provides the overall selectivity of better than 75dB. FL403 also has sufficient selectivity to reject the second image at 910kHz offset.

The IF signal at the output of the second mixer (PIN 3) is processed externally to IC400, by the noise blanker option when this module is fitted to SK401.

Following FL404 are a cascade of limiter amplifiers, within IC400 which is ahead of the FM de-modulator, in the form of a quadrature detector using the tuned circuit of L404. This tuned circuit is adjusted to 455kHz, and a frequency modulated input to this circuit produces the demodulated audio output which appears at PIN9 of IC400.

3.2.1.4 RECEIVE AUDIO PROCESSING

Refer to figure 3.3.

The demodulated audio available at PIN 9 of IC400 is first processed by one stage of the quad OP-AMP IC401. This stage provides three functions:

i) Low pass filter with a cutoff of l00kHz to remove residual 455kHz components of the demodulated audio.

ii) Amplification of the audio signal to an optimum level, approximately 700mV rms for a 60% deviation.

iii) Temperature compensation of audio gain. The temperature compensation is required to ensure a predictable mute circuit operation over a wide temperature range. The output of this OP AMP stage is split into three paths.

3.2.1.4.1 Path 1.

In this path the signal is first attenuated by approximately lOdB with resistors R221 and 8222 on the control board. This is to reduce the AF level into IC204 (the CTCSS decoder and high pass filter), which requires a lower AF level for correct operation. If IC204 is not fitted the option is bypassed by the link 8249, and the signal is then filtered by one stage of the dual OP AMP IC201. This filter is a high pass design with a cut-off frequency of 300Hz. Following the high pass filter is the mute gate circuit using transistors TR202 and TR203. When the microprocessor activates these two transistors the receiver audio signal path is attenuated by more than 70dB. The other stage of OP AMP IC201 acts as an amplifier, with R220 and C215 in the feedback loop, producing a -6dB per octave de-emphasis response.

Some high frequency attenuation above 3kHz is also obtained by the low pass filter action of capacitor C213 and C223 in the audio path.

3.2.1.4.2 Path 2.

The second path of the demodulated received audio, is coupled from the output of IC401 pin 1, to the mute noise processing circuit. A bandpass filter/amplifier using the second stage of IC401 is formed by the combination of L403 and capacitors C461, C462 and C463. With the 25kHz channel spacing version this frequency is 8kHz. For the 12.5kHz channel spacing version additional amplification is required and this is provided by TR427 which has further gain/temperature compensation with R454. The bandpass filter for 12.5kHz version is formed by L403 and C636 at a frequency of 32kHz.

The resulting signal in this frequency band is, effectively, out-of-band demodulated noise.The amplified noise is half-wave rectified at the output of IC401 PIN 14 by diode D426 which is forward biased. The integrator capacitor loading the rectifier is C466. The rectifier configuration actually provides a voltage doubling in the charging of C466.

The third stage of OP AMP IC401 is configured in a Schmitt trigger circuit which compares the voltage across C466 to a reference voltage set by the mute pot R226B on the control board. In the absence of the noise (ie, the receiver is quietened by an incoming signal) the inverting input to the schmitt trigger is biassed at approximately 3 volts. The adjustment range of the mute potentiometer provides the non-inverting input to the schmitt with a voltage between 5 and 7.5 volts. This is always greater than 3 volts, therefore the schmitt output will be high. This schmitt output is voltage divided by D428, R463 and R464 to provide the microprocessor with a +5v logic level to indicate "mute open". When the receiver has no input carrier, the rectified noise increases the voltage at the schmitt inverting input to approximately 6.5volts. This level is limited by D445 and the resistor divider network of R466, R467 and R459. The mute adjust potentiometer may be set to cause a negative difference voltage between the two inputs of the schmitt, in which case the schmitt output will switch low to indicate "mute close" condition. D428 is used to ensure the microprocessor receives 0 volt for the logic low state. D427 in the positive feedback path of the schmitt stage, begins to conduct for the low voltage settings of the mute potentiometer, corresponding to the maximum mute position. This produces a larger hysteresis range for the high mute opening threshold.

3.2.1.4.3 Path 3.

The final path for the demodulated receive audio, is to the pre-processing circuit for the tone sequential signalling decoder.

The signal path of the demodulated audio may also be broken to include the noise blanker circuit option fitted to SK401. When this is done R440 is deleted.

The fourth stage of OP AMP IC401 is used to provide a regulated bias voltage for the other three OP AMPs within this IC.

3.2.1.5 AUDIO OUTPUT

The filtered receive audio is then passed via the volume control to the power amplifier IC202. IC202 may have the output configuration re-arranged to provide a high power (16watV4ohm) output. This results in a bridged output configuration with both speaker connections at roughly half the supply voltage above ground. The speaker is then directly coupled to IC202. The audible alert signal is coupled into the audio power amplifier via resistors R231, R232 and R233. The ratios of these resistors may be set to provide some measure of alert tone generation proportional to the volume control setting.

For systems applications a control input is provided on IC202 at PIN 8 to disable the loudspeaker. Also for special applications, resistor R227 may be selected to provide a minimum volume level feature.

3.2.2 Transmitter

The UHF transmitter power amplifier is shown in block diagram form in figure 3.4. The amplification is achieved in four discrete stages. The first stage has an input of 20mW from the transmit VCO. This becomes amplified by TR417 operating in class AB mode to a level of approximately 200mW. Diode D443 provides temperature stability of the bias for this amplifier stage. The next stage of amplification occurs in TR419 which produces up to 3 watts output. This stage operates in class C mode and the output power is controlled by adjustment of the collector supply voltage. The following stages of TR421 and TR422 provide 10 watts and 30 watts output power respectively, both devices operating in class C. Extensive use is made of micro-strip impedance matching networks between stages. No mechanical tuning of the impedance matching is required.

A power detector circuit at the output of the final power amplifier stage, is realized by detecting the RF voltages appearing at each end of a lumped element equivalent of a quarter-wave transmission line. The quarter wave line comprises L438, C609 and C610. The RF detection is achieved by D438 and C607.

The rectified and filtered voltage is fed back to the inverting input of a comparator circuit using OP AMP IC405. Here, the feedback voltage is compared to an adjustable reference voltage as set by potentiometer R581. The output of IC405 controls the bias voltage to TR420 which in turn adjusts the collector voltage to TR419, and hence the gain of this stage.

The action of this power control loop is to stabilize the output power for a normally matched load.

For a load mismatch condition at the transmitter output, a standing wave will result which causes a higher potential to appear at one end of the quarter-wave transmission section. This will cause a higher detected feedback voltage for the same transmitter power setting. The comparator will correct for this error and the result is a reduction in the output power. Therefore, for most load mis-match conditions the transmitter is protected.The PTC resistor, R579, senses the operating temperature of the transmitter. In the event of a temperature rise above 100 deg C the PTC resistance will increase. This will cause a reduction of the control loop reference voltage and will thereby reduce the transmitter output power, providing a further measure of protection.

A second potentiometer, R578, is used to reduce the reference voltage when low power operation is selected.

The output from the power amplifier is coupled to the antenna socket via a solid state antenna changeover circuit and harmonic filter.

In the receive mode D439, D440 and D441 are all reverse biased through R600. The antenna signal is coupled through to the receiver input. The reverse bias on D440 and D441 in the receive mode ensures a minimum loading on the receiver input by the diodes.

In the transmit mode, +9V is applied to R596 which biases D439 on and couples the output power to the antenna socket. The bias current for D439 flows into D440 and D441 via a PI-section equivalent quarter-wave transmission line. Transistor TR428 is also biassed on, and provides the ground return for diodes D440 and D441. Diodes D440 and D441 are biassed on and form a short circuit across the receiver input to achieve isolation from the transmitter. This short circuit is transformed to an effective open circuit by the action of the quarter-wave transmission line PI section, and therefore does not load the transmitter output. A harmonic rejection low pass filter is placed between the antenna changeover circuit and the antenna socket.

At the output of the antenna changeover circuit, diode D442 which is loosely capacitively coupled to the signal path, rectifies a small amount of the output power. This do voltage is used to bias transistor TR424 on and provides the microprocessor with a signal to indicate transmitter output.

3.2.2.1 VHF POWER AMPLIFIER

The VHF transmitter power amplifier is shown in block diagram form in figure 3.5.
The VHF power amplifier is based on a three-stage line-up utilizing discrete transistors in each stage. The first stage, TR417, operates in class AB mode and amplifies the transmit VCO's 25mW output to approximately 250mW. This stage may have its gain varied by adjustment of the bias voltage at the transistor base input. The second stage of amplification occurs in TR419, operating in class C mode, to deliver up to 3 watts to the final amplifier TR422 which also operates in class C. The output power from this stage is 30 watts to ensure

that 25 watts are available at the antenna socket. Broadband impedance matching circuits are used between all stages with extensive use of printed microstrip.

The output power is stabilized by a power control feedback loop. The power detector consists of a PI-section equivalent quarter-wave transmission line using L432, C594 and C597. The detector is realized by D438 and C593. The do voltage is fed back to the inverting input of a comparator circuit using OP AMP IC405. This voltage is compared to the reference voltage at the non-inverting input which is set by the potentiometer R581. The comparator output voltage provides a control bias current to transistor TR417. The action of this control loop is to adjust the gain of TR417 to maintain a constant transmitter output power.

In the event of a mismatch load at the antenna socket, a standing wave will occur which causes a higher potential to appear at one end of the quarter-wave transmission section. This will cause a higher detected feedback voltage for the same transmitter power setting. The comparator will correct for this error and the result is a reduction in the output power. For most load mismatch conditions therefore, the transmitter is protected.

The PTC resistor R579 senses the operating temperature of the transmitter. In the event of a temperature rise above 100 deg C the PTC resistance will increase. This will cause a reduction of the control loop reference voltage and will thereby reduce the transmitter output power, providing a further measure of protection.

A second potentiometer R578, is used to reduce the reference voltage when low power operation is selected.

The output from the power amplifier is coupled to the antenna socket via a solid state antenna changeover circuit and harmonic filter.

In the receive mode D439, D440 and D441 are all reverse biased. The antenna signal is coupled through to the receiver input. The reverse bias on D440 and D441 in the receive mode ensures a minimum loading on the receiver input by the diodes.

In the transmit mode, +9V is applied to R596 which biasses D439 on, and couples the output power to the antenna socket. The bias current for D439 flows into D440 and D441 via a PI-section equivalent quarter-wave transmission line. Transistor TR428 is also biassed on in transmit mode and provides the ground return for diodes D440 and D441. Diodes D440 and D441 are biassed on and form a short circuit across the receiver input to achieve isolation from the transmitter. This short circuit is transformed to an effective open circuit by the action of the quarter-wave transmission line PI-section, and therefore does not load the transmitter output.

A harmonic rejection low pass filter is placed between the antenna changeover circuit and the antenna socket.

At the output of the antenna changeover circuit, diode D442 which is loosely capacitively coupled to the signal path, rectifies a small amount of the output power. This do voltage is used to bias transistor TR424 on and provides the microprocessor with a signal to indicate transmitter operation.

3.2.2.2 TRANSMIT AUDIO PROCESSING

The majority of the transmit audio circuitry is located on the control PCB. The primary input is at PIN 8 of the microphone input socket SK201. The active microphone derives its power source from the transceiver via the emitter follower transistor TR229. This transistor provides a well decoupled, low noise do supply by effectively amplifying the base capacitance of C301. The supply to the microphone preamplifier is coupled via R311 which also presents the optimum load impedance.

The microphone signal is then processed by one quarter of quad op amp IC210. This stage is configured as a third order high pass filter with a cut-off frequency of 300Hz. Capacitors C307, C308 and C309 set the cut-off frequency. This filter has unity gain and the signal output appears at PIN 1 of IC210.

The input to the next stage passes via the microphone mute gate provided by transistor TR228. When this transistor is activated by the microprocessor, the muting action is achieved by causing the bias point of the OP AMP to be saturated at the output PIN 7 (close to +ve supply).

Following the mute gate is the microphone amplifier stage using another OP AMP of IC210. The input of the microphone amplifier is at PIN 6 and the output appears at PIN 7. This stage may provide more than 30dB voltage gain and adjustment is provided by R322, the microphone gain potentiometer. The output of the microphone amplifier stage may pass directly to the following stage which is a clipper circuit. Alternatively the signal may pass via the CTCSS high pass filter which has the input at PIN 22 of IC204 and output at PIN 20. When CTCSS is fitted IC204 provides additional rejection of low frequency microphone audio below 300Hz, to ensure a minimum disturbance of the CTCSS encode tone. The CTCSS high pass filter provides no additional gain; care must be taken to prevent signal level overload at the high pass filter input.

The resistor divider of R391 and R392 ensure input levels are kept low. The value of the gain setting resistor R377 is chosen to recover the signal loss caused by the attenuator.

At the input to the clipper stage, pre-emphasis is provided by C311 and R324, or when CTCSS is fitted, C247 and R377 provide the pre-emphasis.

The clipper stage provides sufficient gain to cause the output waveform, at PIN 8 of the OP AMP, to reach the limiting levels of the supply voltage and ground. For the OP AMP used this is approximately 8 volts peak-to-peak.

The processed microphone audio is fed to a summing amplifier stage using the remaining OP AMP in the quad package IC210. At the summing point of PIN 13, the microphone audio is combined with the encode signalling options of selective call or CTCSS.
The gain of this summing amplifier is adjusted by R316 which is the deviation setting potentiometer.

The output of the summing amplifier appears at PIN 14 of IC210, this signal passes to the radio PCB via the flexible printed circuit.

On the radio PCB is the final stage of transmit audio processing. The UHF issue C version of this board uses a discrete transistor active low pass filter realized by transistors TR415, and TR416.

This filter is a fourth order low pass with a 3kHz cutoff frequency set by C545, C547, C548 and C549. The output of TR423 emitter connects directly to the transmit VCO for modulation. Trim potentiometer R567 provides an adjustable level to modulate the reference oscillator. This adjustment sets the balance for the two point modulation.

For the VHF and UHF issue E radio PCB assemblies the low pass active filter is realized by a dual OP AMP IC406.

The first stage is configured in a unity gain low pass filter with a cut-off frequency of 3kHz. The output of the filter is at the junction of R564 and C549 and connects directly to the transmit VCO modulation input. The second stage is used as a buffer amplifier to drive the modulation input of the reference oscillator. R567 sets the modulation balance.

3.2.3 Synthesizer

3.2.3.1 GENERAL

The function of the synthesizer is to provide two stable signal sources of high spectral purity. These signals are for the functions of receiver local oscillator and the primary excitation of the transmitter power amplifier.

It is very important to obtain a low single-side-band phase noise for both of these signal sources to achieve the required levels of receiver and transmitter performance.These objectives have been achieved by utilizing a single phase locked loop with a high gain phase comparator and independent receive and transmit low noise VCOs.

3.2.3.2 THE BASIC PHASE LOCKED LOOP SYNTHESIZER

Refer to figure 3.6.

In operation, a voltage controlled oscillator (VCO) produces an output signal at frequency Fo; this frequency is divided down to Fo/N by a programmable divider. A reference oscillator output is also divided down by a programmable divider to produce the synthesizer reference frequency Fr. This frequency is the lowest common denominator which is divisible into all of the required final frequencies (Fo) there are to be programmed. It also becomes the minimum frequency increment of the final frequency.

The signals of Fo/N and Fr are combined in a phase comparator which produces an output voltage proportional to the phase error between these two inputs. The error signal is connected via the loop filter circuit block, back to the voltage control input of the VCO. The error signal causes the VCO frequency to be modified so that no phase difference exists between the two phase comparator inputs. When this occurs the loop is said to be phase locked and Fo/N = Fr.

If the programmable divider value of N is increased by 1 to N+1, then for phase lock to occur Fo'/N+1 = Fr, where Fo' is the new VCO frequency. By simple transposition of this equation it can be shown that Fo' = Fo+Fr. Therefore, by setting Fr to equal the channel spacing, it is possible to select a particular channel by choosing the appropriate value for N, providing of course that the required frequency is within the electronic tuning range of the VCO.

When the synthesizer is used as the transmitter exciter, modulation must also be applied. This is achieved using the two-point modulation technique. The VCO is directly modulated but because this signal will be seen as a phase error which the loop will attempt to correct, it is necessary to apply modulation to the reference oscillator.

The modulation polarity for the VCO and reference oscillator must be the same, ie, a frequency increase of the reference must occur with a frequency increase of the VCO. Test point TP401 is provided to align the modulation balance. When R567 is adjusted correctly the error waveform at the analog phase comparator output will be reduced to a minimum amplitude.

3.2.3.3 THE PRM80 SYNTHESIZER

Refer to figure 3.7.

The phase locked loop synthesizer of the PRM80 consists of discrete transistor voltage-controlled oscillators for both the transmitter and the receiver. Both VCOs have two buffer amplifier stages. The output of each VCO is combined in a passive resistor combining network and a buffer amplifier is provided ahead of the synthesizer frequency divider chain. The frequency dividers consist, of a dual modulus (divide by 64 or 65) prescaler device (Plessey SP8718), followed by the programmable divider IC (Plessey NJ8822). In this integrated circuit are two programmable dividers, one for the division of the VCO frequency, and the other for division of the reference oscillator. The NJ8822 also contains the phase comparator which is provided in two forms, one as a frequency detector and the other as a sample and hold phase detector. The NJ8822 provides the control logic to operate the dual modulus prescaler, and a logic output to indicate the locked state.

The output of the phase comparators are coupled to the loop filter which is realized by half of a low noise dual operational amplifier IC. The other half of the dual OP AMP is used as a tracking circuit to provide an appropriate control voltage for the receiver front end.

The reference oscillator consists of a discrete transistor crystal oscillator, with a voltage control input for modulation. For higher temperature stability, a Temperature Compensated Crystal Oscillator option may be fitted.

3.2.3.4 PRESCALERS AND PROGRAMMABLE DIVIDERS

IC402 is the prescaler.

The purpose of the prescaler is to divide down the operating frequency of the VCO, into a frequency range which is low enough for the programmable divider device which uses low current CMOS technology.

The prescaler is a dual modulus type with programmable division ratios of either 64 or 65. If the prescaler were of the fixed division ratio type (eg: divide by 64), then the frequency steps that may be programmed by incrementing the programmable divider by 1 would be in steps of 64; the total divider chain changing its division ratio by a factor of 64. To program a channel spacing of 25kHz, it would then be necessary to use a reference frequency Fr, of 25kHz/64 = 390Hz.Such a low reference frequency is undesirable because it results in a slow responding loop to frequency changes, less than optimum noise performance, and large division ratios (eg: l0MHz reference oscillator would require a division ratio of 25,600 which is not possible with the NJ8822).

In operation, the dual modulus prescaler division ratio is toggled dynamically by the programmable divider IC403 at PIN 1 of IC402 using +5V CMOS logic. The prescaler's input is at PIN 6 and the divided output appears at PIN 3.

IC403 is the programmable divider and phase comparator IC. The division ratio for both the reference divider and the main frequency dividers are set by a sequence of serial data commands from the microprocessor. The programming inputs at Pins 12, 13 and 14 are serial data, serial clock and chip enable respectively. The programmed data is latched into IC403 and is only updated if a new frequency division is required, or if an out-of-lock state exists. This state appears as a logic high +5V at PIN 4 of IC403. The data is clocked in with a cycle time of approximately 5uSec. The entire data stream occurs in a burst of approximately 150uSec duration. When the loop is out of lock the re-programming occurs every 40mSec. During the burst of data the chip enable input at PIN 14 is held high.

The high gain sample and hold phase comparator has adjustable gain which is set by an external resistor R518 at PIN 17 and capacitor C522 at PIN 15. These components are optimized for each frequency band of the phase locked loop operation. The output of this phase comparator appears at PIN 1 of IC403.

A digital phase/frequency comparator provides for a coarse adjustment of the loop until the VCO frequency is brought within the narrow capture range of the high gain phase comparator. When this happens the output goes into a tri-state condition and appears as a high impedance.

3.2.3.5 LOOP FILTER

The output of the analog and digital phase comparators at PINS 1 and 2 of IC403 are combined at the summing input of the loop filter IC404 is a dual low noise operational amplifier half of which is configured as a low pass filter.The design of this filter determines many of the performance aspects of the phase locked loop. The major aspects being loop cut-off frequency, damping factor, reference frequency suppression, and noise performance. The loop filter is relatively simple and is used primarily to establish the loop dynamics and not to suppress the reference frequency products out of the phase comparator. This is due to the high quality of suppression already achieved by the analog phase comparator in IC403. Although the digital phase comparator at PIN 2 becomes high impedance when in lock, diode D436 is required to isolate the loop filter from any noise residuals of IC403.

The loop filter OP AMP do supply is produced by a voltage tripler circuit on the control board. This 23 volt supply enables the loop filter output to control the varicap diodes of the VCO and receiver front end over a wide capacitance range. Using the higher control voltage on the varicaps is preferred to using tighter varicap coupling, which would result in noise degradation.

To improve the signal-to-noise ratio of the OP AMP output control voltage, it is necessary to maintain the voltage above 7 volts. This is achieved by a switched voltage divider using R532 and R533. For channel frequencies in the lower 1/3 of the operating frequency band, transistor TR414 is activated by the microprocessor to switch in the voltage divider. This causes the loop to increase the OP AMP output voltage so as to maintain the correct control voltage on the VCO. The divider circuit is switched out for channel frequencies above the 1/3 of band point.

Resistors R532 and R533 are metal film to minimize control voltage noise.

The second half of the dual OP AMP IC404 is used to provide a tracking voltage for control of the receiver front end. The tracking voltage range is adjusted by the tracking gain potentiometer, R557, and the offset is adjusted by the tracking offset potentiometer R554. These adjustments are set to ensure that the centre frequency of the receiver front end tracks the tuning of the local oscillator VCO.

3.2.3.6 REFERENCE OSCILLATOR

Transistor TR413 is configured in a modified Pierce oscillator circuit using a quartz crystal XL401 in the feedback path. Feedback occurs between the base and collector of TR413 which provides 180 degree phase shift. The crystal operates in a parallel resonance mode to provide a further 180 degree phase shift. The oscillator is tuned to the correct frequency of 10MHz by a tunable coil, L411, placed in series with the crystal. Varicap diode D435 which is also in series with the crystal is reverse biassed to approximately 4.5 volts. The transmit audio is ac-coupled to this diode by C542, as part of the two-point modulation technique.

The oscillator output of approximately 1.5 volt peak-to-peak is connected to the programmable reference divider at PIN 9 of IC403. The reference oscillator signal also appears at PIN 10 of IC403 at a level of 5 volt peak-to-peak.

For extended temperature operation down to -30 Deg C, a crystal heater is employed. Transistor TR425 is activated when the transceiver is switched on and passes current through the positive temperature coefficient resistor R620.

The PTC has intimate thermal contact with XL401. For temperatures below approximately 0 Deg C the resistance reduces and more current is drawn. This results in self heating of the PTC. The effect is to maintain a crystal temperature of not less than -10 Deg C for ambient temperatures below 0 Deg C.

For higher temperature stability than is achieved with a standard crystal, a temperature compensated crystal oscillator (TXCO) option may be fitted. When XL402 is fitted the discrete reference oscillator, using TR413 and XL401, is not used. Adjustment of the frequency of the TCXO is provided on the module.

3.2.3.7 VOLTAGE CONTROLLED OSCILLATORS

The UHF voltage controlled oscillators for the transmitter excitation, and the receiver local oscillator function, make use of ceramic coaxial resonators. These resonators are, effectively, a quarter-wave transmission line with one end short circuited. The other end of the resonator appears electrically as a parallel L-C tuned circuit with a very high Q. The resonator is used in a Colpitts oscillator configuration with TR406 as the receive oscillator and TR410 as the transmit oscillator.

In the receive VCO, varicap diode D431 provides the voltage control with the bias voltage supplied through L405. The main voltage control for the transmit VCO is provided by varicap diode D434. Varicap diode D433 is very lightly coupled to the resonator of the transmit VCO, to provide the modulation input.

An active power supply filter circuit is used for each oscillator, to suppress noise voltages on the regulated supply. In the receive VCO C470 provides the main bypass capacitor for this active filter, and diode D430 ensures rapid charging when the oscillator power supply is switched on.
No mechanical adjustments are required for alignment of the VCOs.

A two-stage buffer amplifier is incorporated on each VCO to ensure adequate isolation and thereby minimize any frequency pulling effect with load variations. These buffer stages also provide sufficient output power to drive the synthesizer and the other following circuits (mixer for the receiver, and the transmitter power amplifier).

The oscillator and buffer amplifier stages, are housed in separate screened compartments which are provided by the die-cast radio screen. This ensures a very high immunity to microphony, and aids in isolating the VCO from the frequency pulling effects due to load variations.

The VHF voltage-controlled oscillators for the transmit and receive function use parallel L-C tuned circuits as the resonant element. The tuned circuit is configured in a grounded gate modified Colpitts oscillator, using a JFET transistor.

The receiver oscillator using transistor TR406 is nominally tuned at the highest required frequency by adjustment of L407. The varicap diode, D431, electronically tunes the VCO to cover the entire frequency band. An active filter using transistor TR405 and C470 as the main bypass capacitor, provides the oscillator with a low noise, stable regulated supply voltage.

In the transmit VCO an additional varicap diode, D433, is lightly coupled to the tuned circuit to provide the modulation input.

Both the transmit and receive VCOs have a two-stage buffer amplifier.
In the receive VCO the first buffer stage uses a dual gate mosfet TR407. The oscillator signal appearing at the source of TR406 is voltage divided by capacitors C487 and C488, and amplified by the first buffer stage. A second buffer amplifier stage, using a common emitter bipolar circuit with TR408, provides additional gain and isolation for the VCO. The power

output produced by each buffered VCO is sufficient to drive the synthesizer frequency divider and the other following circuits, (mixer for the receiver and the transmitter power amplifier). The VCO and buffer stages for both transmit and receive oscillators, are housed in separate screened compartments which are provided by the diecast radio screen. In this way a very high immunity to microphony is assured.

3.2.4 Central Control

Refer to figure 3.9.

3.2.4.1 GENERAL

Refer to the simplified block diagram figure 3.1 and also to circuit diagram for detailed description. The PRM80 central control consists of a dedicated single chip microprocessor IC206. This device supervises all functions of the transceiver as well as providing the analogue selective call encode and decode. The microprocessor is located on the control printed circuit board, in conjunction with the associated power supply and peripheral circuits. Interface between the microprocessor and the controlled functions is via a bi-directional serial data bus. The nature of this data control is such that the bus is inactive unless a specific action is required, eg. re-program synthesizer, change display information, etc. To effect control via the serial bus, the integrated circuit under control is enabled during the period of the data burst.

All the operational characteristics of the software are fixed in the masked program memory within the microprocessor. The external EEPROM is required to provide the microprocessor with information on which software options are to be enabled from the many configurations available.

3.2.4.2 POWER SUPPLY

The radio transceiver uses five supply voltages in all, four of which are provided as regulated voltages. The supply voltages are:

+13.8V unregulated
+5.2V regulated (switched)
+5V regulated (un-switched)
+9V regulated (switched)
+23V regulated (switched)

The unregulated +13.8V supply connects permanently to the transmitter power transistors TR421 and TR422, and also to the receiver audio power amplifier IC202. This primary supply voltage is filtered by L205 and C285, C286. A high power Zener diode, D217, provides for suppression of voltage spikes and reverse polarity protection.

The +5.2V regulated supply operates all the logic controlled integrated circuits. The +9V regulated supply operates the majority of the radio and audio analogue circuitry. The +23V supply is used to power the synthesizer loop filter OP AMP and the front end tracking circuit.

A low current +5V regulator operates permanently to supply the microprocessor internal RAM.

The microprocessor derives its power from the +5.2V regulated source via D216, the remaining logic controlled devices are supplied power via D221. The nominal +5V regulator has its output boosted to 6 volt by means of the voltage divider R336 and R337 and the diode D215. Diode D215 is incorporated to provide temperature compensation. The slightly higher than usual +5.OV supply is required for correct operation of the prescaler integrated circuit IC402 which also operates off this supply.

When the transceiver is switched off, standby power is only supplied to the microprocessor and reset circuit, via D219 from the Zener diode regulator formed by D218 and R290. Diode D216 effectively isolates this standby supply.

At the output of the +9 volt regulator, IC209, are three series pass transistors TR216, TR218 and TR219. TR218 and TR219 are controlled by TR220 which in turned is controlled by the microprocessor via the latch IC207. When the transceiver is in the receive mode TR220 is switched off and so is TR219. TR218 derives forward bias via D220 and R297 to ground. With TR218 switched on the 9 volt regulated supply is connected to the receiver related circuitry.

When the transceiver PTT is activated, the microprocessor switches TR220 on via the Tx enable on PIN 14 of the latch IC207. This biases TR219 on and in doing so deprives TR218 of base current, via D220, to turn TR218 off. The transmitter circuitry is powered via TR219 and the receiver supply is disabled.

To activate the transmitter power amplifier the microprocessor provides a separate control output, PA enable, via the latch IC207 at PIN 7 to enable transistor TR217. When TR217 is enabled TR216 is biased on and supplies the transmitter buffer stage TR417 with power. A timing delay of 40mSec is provided between +9V Tx and +9V PA output, to ensure the synthesizer frequency has settled before the transmitter power amplifier is activated. When the transmitter is disabled the +9V PA is switched off lOmSec before the +9V Tx supply is switched off. This also ensures the synthesizer remains on the transmit frequency until the transmitter power output has ceased.

Transistor TR221 is provided as a transmit inhibit switch and is controlled by the synthesizer lock detector. If the synthesizer is out-of-lock the base of TR221 is forward biased which disables the PA enable control to TR217. This ensures that the transmitter is never activated during an out-of-lock condition.The +23V supply is generated by voltage tripling the +9V supply using a multivibrator circuit. Two NAND gates from IC200 are configured as a multivibrator circuit with the frequency of 300kHz set by R200 and C200. The output at PIN 10 of IC200 is a 9 volt peak-to-peak square-wave which is used to alternately switch TR200 and TR201. These two transistors have different voltage dividers at the base to ensure that only one transistor will be conducting at any time. The transistors effectively boost the current output drive of the multivibrator.

The resulting square-wave appearing at the junction of TR200 and TR201 collectors is coupled to a voltage multiplying rectifier comprising C202, C203, C205, C206, D200, and D201.

The circuit requires several changes of state of the switching transistors before the output voltage reaches +23V However, assuming a loss-less circuit with the oscillation starting with TR201 conducting and TR200 off, then all capacitors C202, 0203, C205, C206 are charged to approximately +9V

On the second cycle when TR200 is on with TR201 off, both C205 and C206 have their charge pumped to +18 volt due to the charge transfer from C202 and C203 respectively. C202 and C203 maintain their +9V charge in this cycle.

On the third cycle with TR201 on and TR200 off, C203 has its charge pumped to +18V by the charge transfer from C205. C202 maintains its charge to +9V by current flowing from +9V supply down through D200.

On the fourth cycle with TR200 on and TR201 off, C206 has its charge pumped to +27V by charge transfer from C203. During this cycle C205 maintains its charge at +18V by charge transfer from C202.

In practice, circuit losses and diode voltage drops result in +23 volt output rather than +27V and the circuit takes more than 4 cycles to reach full voltage. However, because of the high oscillation frequency the +23V output is available in less than 1mSec from application of the +9V supply.

A high current 9-volt supply for the LCD backlighting is provided by TR215 which obtains its bias voltage from TR214. In special systems applications it is necessary to provide the microprocessor with an indication of the power off status although the equipment is permanently powered on. This is provided by the output of the voltage divider R365, R366 connected to PIN 20 of the microprocessor. In the permanent power configuration link LK201 is fitted and LK202 is removed.

3.2.4.3 RESET

The PRM80 reset circuit monitors the radio supply voltage and performs the following functions.

i) Disable the radio for supply voltages less than 9.8 volts. Resume operation for supply voltages of greater than 10.2 volts.

ii) Generate an interrupt signal for the microprocessor during a low voltage condition.

iii) Generate a reset signal for the microprocessor after recovery from a low voltage condition.

When the supply voltage is 13.8 volts, 5.1 volts is dropped across D225 leaving 8.7 volts across R300. TR224 base emitter is reverse biased and D226 is conducting, hereby, limiting this reverse bias. TR224, TR225, TR226, TR227 and TR232 are all biased off.

Therefore, the RESET output of the collector of TR227 is low (0 volt) and the interrupt at the collector of TR225 is high (+5.2 volt). In this state the microprocessor is active.

When the primary supply voltage drops below 9.8V, the voltage drop across D225 allows R300 to forward bias TR224. TR224 and TR232 form a Schmitt trigger with R395 providing hysteresis and C302 providing speed up. As TR224 collector voltage rises, TR232 also conducts, reinforcing TR224 forward bias. TR225 is biased on, generating a logic low (0 volt) on the microprocessor interrupt input PIN 8. During this interrupt state, the majority of the microprocessor ports are set low and the microprocessor is configured in a low current consumption standby mode. All operational aspects of the radio are also disabled.

The instant at which the interrupt active low output occurs, TR232 collector switches low. This causes TR226 to forward bias and its collector raises the base voltage of TR227, to ensure that the RESET output at the collector of TR227 remains low. This mechanism ensures that the RESET is never active during the time the interrupt is active for the power failure condition. The low collector voltage of TR232 also causes C299 to discharge via D227 and R302.

Immediately following the initial supply voltage application TR224 switches off. TR225 and TR232 also switch off, and the interrupt control to the microprocessor becomes inactive (+5.2V). The RESET output at the collector of TR227 switches to active high (+5.2V). This is held for 120mSec until C299 charges. During the RESET period with interrupt high and reset high, the microprocessor output ports are configured to logic high.

Upon initial power application conditions may occur where the interupt becomes active low until the supply voltage has increased sufficiently to switch off TR224. In this case the RESET output must be held high. TR233 is active during the initial power-up and ensures that TR226 is biassed off and, thereby, TR227 conducts for the period of the time constant set by C299.

If a supply voltage interruption occurs during the 120mSec RESET period, TR224, TR232 and TR226 are instantly switched on, causing the RESET output at the collector TR227 to switch low. C299 is also discharged and will re-initialize the 120mSec timer for the RESET output pulse. The interrupt output is delayed following the reset by R394 and C298 to allow the microprocessor to prepare for the interrupt.

3.2.4.4 CLOCK

The 16MHz clock signal for the control microprocessor is derived from the crystal oscillator composed of TR211, XL201 and associated components. The frequency of this oscillator can be shifted approximately 500ppm by switching the crystal capacitance via TR212 and C281. Control of this switching is by the central control processor on a per channel basis via the serial latch IC207 pin 12. Oscillator switching is provided to reduce possible receiver desensitisation due to harmonics from the 16MHz clock and its associated subharmonics.

The buffered output of the clock from the control processor is fed to IC211 and is then divided by 16 to produce the 1 MHz clock required by IC204, the CTCSS encoder/decoder.

Later models will have a 12MHz clock oscillator, which requires different hardware and software.

3.2.4.5 RADIO INTERFACE TO MICROPROCESSOR

The interface between the radio system and the microprocessor occurs in three ways, by the microprocessor directly, by the microprocessor serial control bus, or by the serial latch IC207. The microprocessor port connections are configured as either; inputs only, outputs only, or, in the case of the serial bus, as a bi-directional port.

The following is a description of the ports and their allocated function:

P0.0 Keyboard row 1
P0. 1 Keyboard row 2
P0.2 Keyboard row 3
P0.3 Microphone cradle input
P0.4 Microphone PTT input
P0.5 Hardware mute input
P0.6 Synthesizer out-of-lock input
P0.7 CTCSS detect input

All the above port lines are configured as inputs.

Lines P0.0, P0. 1 and P0.2 are used to read to which row the pressed key belongs. This is used in conjunction with ports P3.5, P3.6 and P3.7.

Line P0.3 comes from the microphone socket pin 3 via a suppression network consisting of C269, R281 and R277. This input is active low ie: a 0V level indicates microphone-in-cradle. Line P0.4 comes from the microphone socket pin 4 via a suppression network consisting of C270, R282 and R278. This input is active low, ie: a 0V level indicates transmit, and a high level 5V indicates receive.

Line P0.5 comes from the hardware mute detector circuit. It is used to indicate to the control program the presence or not of an RF carrier on the channel, ie: a 0V level indicates no RF carrier.

Line P0.6 is the phase locked loop synthesizer out-of-lock indicator line. This signal comes from IC403 on the radio PCB and indicates to the control program whether or not the synthesizer is in-lock, ie: a 0V level indicates in-lock.

Line P0.7 is derived from the CTCSS encoder/ decoder IC204. This signal indicates that the CTCSS decoder is decoding the correct sub-audible tone, ie: a 0V level indicates CTCSS decode.

P1.0 Serial control bus data line
P1.1 Serial control bus clock line
P 1.2 LCD display driver enable
P1.3 PLL synthesizer program enable
P 1.4 EEPROM enable
P 1.5 CTCSS encoder/decoder enable
P1.6 Radio latch enable
P1.7 Radio latch output enable

Port 1 of the control processor is primarily the serial control port which controls the various serial control devices within the mobile.

P1.0 is the serial data line. This line may be used as either an input or an output depending on which serial device the control processor is communicating with. It is configured as an output when communicating with the display driver, CTCSS IC, serial latch, RF synthesizer and writing to the EEPROM. It is configured as an input when reading from the EEPROM.

P 1.1 is the serial clock line. It is always configured as an output and is active whenever the control processor is communicating with any of the serial devices.

P1.2, P1.3, P1.4, P1.5, P1.6 are the select lines for each of the serially controlled devices. They are always configured as outputs. These ports are high whenever the associated serial device is being addressed.

P1.7 is used to disable the outputs of the serial latch IC207during power up and power fail conditions. It ensures that the devices controlled by IC207 are disabled for the duration of the above conditions.

P2.0 External alarm input
P2.1 RF power detect
P2.2 Alarm power sense
P2.3 3rd party option toggle
P2.4 CTCSS encode RTB control
P2.5 Analogue signalling control
P2.6 Analogue signalling control
P2.7 Analogue signalling control

The external alarm input from SK203 pin 4 goes via R248, and bypass circuitry composed of C235 and D204, to P2.0 of the micro controller. This pin is normally pulled up by R247 to a logic high level. It must be grounded to activate the alarm.

P2.1 is the RF power detect input. This signal is derived from the radio board when logic low indicates that RF power is present at the radio RF power amplifier.

P2.2 is the alarm power sense line. When the alarm is activated this line is used to determine the state of the on/off switch in order that the correct display may be maintained.

P2.3 is a port which has been set aside for the controlling of items external to the control PCB. When this function has been programmed this line will toggle on and off in response to the activation of the relevant front panel button.

P3.0 Serial programming received data
P3.1 Serial programming transmit data
P3.2 Low volts interrupt
P3.3 Analogue signalling interrupt
P3.4 Alert tone generator control
P3.5 Keyboard column 1
P3.6 Keyboard column 2
P3.7 Keyboard column 3

P3.0 is the serial programmer receive data line. P3.1 is the serial programmer transmit data line.

P3.2 is the low volts interrupt input. When the supply voltage to the mobile drops below 9.8 volts this pin will go to a logic low level.

P3.3 is the analogue signalling interrupt input pin. This pin will have a series of pulses approx 20uSec wide appearing on it.

P3.4 controls the alert tone generator. A logic low from this output will turn on the alert tone generator.

Lines P3.5, P3.6 and P3.7 are used to set each column low in turn so that the pressed key may be read by ports P0.0, P0. 1 and P0.2.

3.2.4.6 SERIAL LATCH

The serial latch IC207, controls the following radio functions.

Q0 Transmit power control
Q 1 Receiver mute control
Q2 External alarm output
Q3 Transmit PA enable
Q4 Transmitter enable
Q5 Microphone mute control
Q6 Crystal oscillator shift control
Q7 Synthesizer switch control

Q0 is the transmit power control line. A logic 0 level on this line indicates high transmitter power. A logic 1 level sets the transmitter for low power.

Q1 is the receiver mute control. A logic 1 on this line mutes the received audio.

Q2 is the external alarm output. This output controls an open collector transistor.

Q3 is the transmitter power amplifier enable. A high level on this pin will enable the transmitter.

Q4 is the transmitter enable line. When this line is at a logic high level the 9-volt power to the receiver is disabled and the 9-volt power to the transmitter is enabled.

Q5 is the microphone mute line. A logic 1 level on this line mutes the transmit audio.

Q6 is the crystal oscillator shift line. When this line is high the frequency of the crystal oscillator is moved in frequency by -500ppm.

Q7 is the synthesizer switch line. This line is used to lower the noise output of the synthesizer control loop.

3.2.4.7 SERIAL CONTROL BUS

The serial control bus is used for control of the following devices; EEPROM, display driver, CTCSS encoder/decoder, serial latch and the RF synthesizer. Each of the serial devices is accessed by asserting an enable line and then serially clocking the data into the chip.The control of each device is as follows:

3.2.4.7.1 EEPROM

IC203 is an electrically erasable programmable read only memory which contains the configuration information of the mobile independent of any power supply. Apart from the microprocessor, the EEPROM is the only device on the serial data bus which is able to both send and receive data. The 9- and 64-channel variants have a 256 byte and 512 byte device respectively. The devices are configured as 128 by 16 and 256 by 16 respectively but as they are communicating with an 8-bit micro controller, the control program treats the devices as 8-bit arrays.

When programming the EEPROM, as occurs in initial configuration of the equipment, the following steps occur. First the EEPROM is sent a write enable command. This consists of the enable line to the device going high and then the write enable command is clocked into the device using the serial clock and data lines. 9 bits of data are clocked in. The enable line is then returned low.

Next, the data to be written to the EEPROM along with the program command is clocked into the device. This consists of 28 bits of data and command information. While the device is internally programming, the data out line (serial data) indicates the state of programming. This data out line is low while programming and high when programming is completed. This programming typically takes 5 to 10 mSec. When all this is finished, a write disable command of the same form as the write enable command is issued to the device. Reading of the data in the EEPROM is accomplished by setting the enable line high and then clocking in the read command and address.

Next the data of that location is clocked out, and the enable line is then returned to 0. There are 4 different read modes used in the PRM80. When reading a byte then only 8 bits of data are clocked out before de-selecting the device. When reading 16 bits then the whole 16 bits are clocked out.

When reading channel data the read command, address and then 48 bits of data are clocked out. When changing channel and an invalid channel is selected then only the read command, address and two bits of data are clocked out. If the channel data is valid then the 48 bits of data will be clocked out.

3.2.4.7.2 Display Driver

The display driver, IC100, is the same for both the 9- and 64-channel variants. The display IC is programmed by first setting the enable line high and then clocking in 21 bits of serial data using the clock and data lines. The enable line is then returned to the low level. Two groups of data are required for the display driver, one group for each back plane of the LCD. The 9-channel device only utilises one back plane so there will only be one group of data sent to

the display, whilst the 64-channel variant utilises both back planes and thus requires two groups of data. Note the period of the serial clock when addressing the display driver is approx 10 times greater than that required for the other serial devices.

3.2.4.7.3 CTCSS encoder/decoder

The CTCSS encoder/decoder is programmed in the period following the synthesizer programming while waiting for the synthesizer loop to lock. It is programmed by first clocking out 8 bits of serial data using the clock and data lines. Next a load pulse is applied to the device and the new data is latched in.

3.2.4.7.4 Serial Latch

The serial latch is programmed by first clocking out 8 bits of serial data using the clock and data lines. Next a load pulse is applied to the device, the serial data is latched in and the outputs change.

3.2.4.7.5 Synthesizer

The synthesizer on the radio pcb is serially programmed by the main control processor. The clock, data and enable signals are provided from ports PLO, P1.1 and P1.3 of IC206. These logic control signals are directed via D207, D208 and D206 which prevent noise from the micro processor being coupled to the RF synthesizer. When the synthesizer is being programmed by the control processor the enable line is set to a logic high level. Then a series of 29 clock pulses along with 29 bits of data are serially clocked into the synthesizer IC. Finally the enable line is returned to the logic low level. The clock pulses will typically be of luSec duration. Some pulses may appear to be stretched but this is due to the operation of the control processor, and is normal. The rate at which the synthesizer is reprogrammed is dependent on the mode of operation of the mobile. If the synthesizer is out-of-lock then the control processor will attempt to reprogram the synthesizer approximately every 40mSec. Whereas if the mobile is scanning with CTCSS selected it may be as long as 400mSec between successive reprogramming of the synthesizer.

3.2.4.8 SELECTIVE CALL SIGNALLING

The selective call signalling in the PRM80 is achieved by means of a software control program operating in the main control micro processor for both encode and decode functions. During decode operation the pre-emphasised receive audio from the receiver is filtered by the bandpass filter consisting of IC205a. This filtered audio is then passed to the zero-crossing detector consisting of IC205b, IC205c, TR207, TR208, C249, C250, R261 and R262. During positive signal input the output of IC205 goes logic high. This logic high is then coupled via C250 to the base of transistor TR208 turning it on for a period of approx 20uSec. Resistor R262 ensures that TR208 turns off and also effects the length of the pulse. The collector of TR208 then pulls down resistor R260 to logic 0 level for this short period. For negative signal input the same process occurs with IC205c, C249, TR207 and R261. Thus there is a logic 0 pulse for every zero crossing of the input signal. The series of pulses produced is applied to the interrupt pin of the main control processor, IC206 for processing.

During encode operation the output ports P2.5, P2.6 and P2.7 are controlled by the microprocessor. The outputs from these ports are combined by the summing network consisting of R267, R268 and 8269. This signal is then integrated and filtered by IC205d and its associated components. The output of IC205d is then coupled via C263, R323 and R390 to the final transmit audio summing amplifier IC210.

3.2.4.9 CTCSS AND REVERSE TONE BURST

IC204 located on the control PCB, is the CTCSS encoder/decoder device. When this option is fitted R249 is removed and the receiver audio signal path is passed via IC204 at PINS 23 and 19. The audio output at PIN 19 is high pass filtered by IC204, to remove frequencies below 300Hz. This ensures that received signals containing the sub-audible tones have the tones removed to prevent unnecessary residual hum at the loudspeaker.This audio path through IC204 is muted until a tone is successfully detected or the microprocessor provides an unmute command to IC204.

The audio input at PIN 23 of IC204 is also processed to decode the CTCSS tone. When a tone is successfully decoded the output at PIN 13 is switched to a logic low, and the received audio is passed.

A microprocessor command changes IC204 from decode to encode when the PTT is activated on a CTCSS channel. The encode tone output appears at PIN 16 at a level of approximately 775mV rms. The encode tone output has two alternate paths before being combined with the transmitter audio at PIN 13 of IC210. One path passes via C243 and the CMOS switch IC212 to the encode level setting potentiometer R354. The alternate path is via transistors TR230 and TR231. This circuit provides the -120 deg RTB feature. The passive network of C241, C242, R344 and R345 produces approximately 60 deg phase lag. TR231 provides a further 180 deg and this combination results in a total of 120 deg lag. During a transmission the encoder tone output passes via C243 to PIN 1 of IC212. The output appears at PIN 2 and 3. Microprocessor control sets IC212 PINS 13 and 6 to logic high. At the release of PTT, IC212 PINS 13 and 6 are switched low by the microprocessor and the encode tone is passed via the phase shift network to PIN 4 of IC212 and this signal now appears at PINS 2 and 3 of IC212.

An alternative 180 deg RTB is available directly from IC204 output. When 180 deg RTB option is required the microprocessor provides IC204 with a serial command to produce a 180 deg phase shift in the encode tone. In this option the encode output is passed via C243 and IC212 but the -120 deg phase shift network is never activated.

3.2.5 Front Panel

3.2.5.1 9-CHANNEL FRONT PANEL

The visual information is displayed on the Liquid Crystal Display LCD 1. A seven-segment symbol may display up to channel digit number 9. Other visual indicators are as follows:

Receiver Busy
Transmit
Selcall (call or called)

Scan
Button Chevron

LCD 1 is electrically connected to the driver integrated circuit IC 100 by a zebra strip. This IC contains an internal clock with the frequency set by resistor R104 and capacitor C100. This clock provides the strobe for the backplane of the LCD.Display information is programmed into the driver IC from the control microprocessor. The information is programmed serially with the enable input at PIN 28 of IC held high during the data burst. The information is latched within IC100.

Backlighting of the LCD is provided by a single incandescent bulb LP101, which is illuminated when the transceiver is switched on.

The 9-channel front panel has four push buttons which are arranged in a matrix configuration and connected to the microprocessor via four inputs.

3.2.5.2 64-CHANNEL FRONT PANEL

The visual information is displayed on the Liquid Crystal Display LCD 1. The two seven-segment symbols provided display up to channel number 64. An additional two seven-segment symbols are provided to display up to status number 99 for selective call signalling. Other visual indicators provided are as follows:

Receiver Busy
Transmit
Selcall (call or called)
Scan
Auxiliary 1
Auxiliary 2
Button Chevron

LCD 1 is electrically connected to the driver integrated circuit IC 100 by a zebra strip. This IC contains an internal clock with frequency set by resistor R 104 and capacitor C 100. This clock provides the strobe for driving the backplane of the LCD.

Display information is programmed into the driver IC from the control microprocessor. The information is programmed serially, with the enable input at PIN 28 of IC 100 held high during the data burst. The information is latched within IC100.

Backlighting of the LCD is provided by two incandescent bulbs LP101 and LP102, which are illuminated continuously when the transceiver is switched on.

The 64-channel front panel has eight push-buttons which are arranged in a matrix configuration and connected to the microprocessor via six inputs.

3.2.5.3 KEYBOARD

The keyboard of the 9-and 64-channel variants use a similar matrix. In the 9-channel variant only 4 positions are scanned whereas in the 64-channel variant the 9 positions are scanned.

One position is unused in the 64-channel variant. In operation each column line is, in turn, set to a logic low level. As each column is scanned the row lines are read by the port 0 lines to determine if any keys on that particular column have been pressed. This occurs for each of the three rows and the control program is then able to determine which key has been pressed and what action to take. When a pressed key is detected it is debounced by reading the matrix a number of times to ensure that only one key press is registered. Some keys have been designated as auto-repeating keys, in which case once the auto-repeat sequence has been entered the matrix will be read at the auto repetition rate.

SECTION 4 ALIGNMENT PROCEDURE

4.1 TEST EQUIPMENT

i) Rhode and Schwartz model SMFP or CMT. Alternative:
Marconi transceiver test set model 2995.

ii) Power supply 13.8 volt at 10 amp
Kenwood PD35-20 or PS775.

iii) CRO Philips PM3055 (greater than 20MHz BW).

iv) DVM Fluke 77 or similar

4.2 GENERAL INSTRUCTIONS

i) The alignment of the PRM80 is performed using the EEPROM customization memory programmed with the standard test and alignment information.

ii) A non-metallic tuning tool should be used for all tuning coil adjustments, and an insulated tool for all other adjustments where short circuits could occur.

iii) The negative lead of all test equipment should be connected to the PRM80 chassis unless stated otherwise.

iv) This alignment procedure assumes that the equipment is operating normally and is without faults.

4.3 PRELIMINARY ADJUSTMENTS

i) Ensure test frequencies and options are programmed into the EEPROM. This program is for functional test and alignment purpose only.

ii) Remove the radio screen if fitted.

iii) Adjust the rotary volume and mute controls fully counter-clockwise.

iv) Preset VHF front end tuning cores. Fiush with end of former. (see figure 4.2).

v) Set the supply voltage to 13.8Vdc. (measured at do supply socket connection).

4.4 TEST FREQUENCY TABLE

NOTE; The appropriate table of information should be programmed into the transceiver.

Frequency Band (MHz)	Channel Number	Test Frequency (MHz) TX	Rx	OPTION DETAILS Transmit	CTCSS	Selcall
EO 68 to 88	1	68.025	68.525	25		
	2	78.025	78.525	25		
	3	87.025	87.525	25		
	4	68.025	68.525	1	107.2Hz	
	5	78.025	78.525	1	107.2Hz	ENC test
	6	87.025	87.525	1	107.2Hz	
BO 132 to 156	1	132.025	132.525	25		
	2	140.025	140.525	25		
	3	155.025	155.525	25		
	4	132.025	132.525	1	107.2Hz	
	5	140.025	140.525	1	107.2Hz	ENC test
	6	155.025	155.525	1	107.2Hz	
A9 146 to 174	1	146.025	146.525	25		
	2	160.025	160.525	25		
	3	173.025	173.525	25		
	4	146.025	146.525	1	107.2Hz	
	5	160.025	160.525	1	107.2Hz	ENC test
	6	173.025	173.525	1	107.2Hz	
Tm 400 to 440	1	400.025	400.525	25		
	2	420.025	425.525	25		
	3	439.025	439.525	25		
	4	400.025	400.525	1	107.2Hz	
	5	420.025	420.525	1	107.2Hz	
	6	439.025	439.525	1	107.2Hz	ENC test
U0 440 to 470	1	440.025	440.525	25		
	2	455.025	455.525	25		
	3	469.025	469.525	25		
	4	440.025	440.525	1	107.2Hz	
	5	455.025	455.525	1	107.2Hz	
	6	469.025	469.525	1	107.2Hz	ENC test

Frequency Band (MHz)	Channel Number	Test Frequency (MHz)		OPTION DETAILS		
		Tx	Rx	Transmit Power	CTCSS ENC/DEC	Selcall
W1 470 to 500	1	470.025	470.525	25		
	2	485.025	485.525	25		
	3	499.025	499.525	25		
	4	470.025	470.525	1	107.2Hz	
	5	485.025	485.525	1	107.2Hz	
	6	499.025	499.525	1	107.2Hz	ENC test tone
W4 500 to 520	1	500.025	500.525	25		
	2	510.025	510.525	25		
	3	519.025	519.525	25		
	4	500.025	500.525	1	107.2Hz	
	5	510.025	510.525	1	107.2Hz	
	6	519.025	519.525	1	107.2Hz	ENC test tone

4.4.1 Selcall Encode Test

Program detail:	CML CCIR	
Lead-in-Delay	9999mSec	
Lead-in-Tone	Required	
Lead-in-Tone 4	(1358Hz)	
Individual Encode Identity (1)	1, 2, 3, 4, 5	40mSec
Individual Decode Identity	1, 2, 3, 4, 5	40mSec
Group Decode Response	Normal Alert	

Note; CTCSS encode only on channel 5 VHF, and channel 6 UHF.

4.5 THE PROCEDURE

4.5.1 VCO Alignment

4.5.1.1 VHF RECEIVE VCO

Step No	Result Measured by	Result Measured at	Adjust	Result	Notes
1			Switch on power Select ch. 3..		Highest freq. channel.
2	DVM, dc volt, range	TP402	L407	15.0 +10.2V	
3	DVM, dc volt. range	TP402	Select channel 1	3.OV to 5.OV	Lowest freq. channel.
4			Disconnect DVM.		

4.5.1.2 VHF TRANSMIT VCO

Step No	Result Measured by	Result Measured at	Adjust	Result	Notes
1			Switch on power. Select ch. 3.		Highest freq. channel
2			Activate PTT.		
3	DVM, dc volt. range	TP402	L445	15.0 -/+ 0.2V	
4			Disable PTT		
5	DVM, do volt. range	TP402	Select ch. 1 and activate PTT	3.0 to 5.0V	Lowest freq. ch.
6			Disable PTT Disconnect DVM		

4.5.2 Transmitter Power Adjustment

Step No	Result Measured by	Result Measured at	Adjust	Result	Notes
1			Switch on power. Select ch. 2.		Mid freq channel for high power
2			Activate PTT		
3	Power Meter	Antenna socket	R581	25.0 -/+ 1 watt	

4.5.2 Transmitter Power Adjustment (Continued)

Step No	Result Measured by	Result Measured at	Adjust	Result	Notes
4	Ammeter	do supply input		<6.5A (UHF) <5.5A (VHF)	Checks current consumption
5	LC Display				Ensures Tx indicator is operating
6			Disable PTT select ch. 5		Mid freq. channel for low power.
7			Activate PTT		
8	Power Meter	Antenna socket SK402	R578	1.0 -/+ 0.1 watt.	
9	LC Display				Ensures Tx indicator is operating.
10			Disable PTT		
11	Transmit Power must be re-adjusted when the radio screen is fitted. See 4.5.7, step 10				

4.5.3 Reference Oscillator Tuning

Step No	Result Measured by	Result Measured at	Adjust	Result	Notes
1			Switch on power		Perform alignment 4.5.2 if not already completed.
2			Select ch. 2		Mid freq. channel.
3			Activate PTT		
4	Frequency counter	Via power meter at antenna socket SK402	L411	+/- 500Hz of correct frequency	Check for correct freq in table 1. (Sect.4.4)
5			Disable PTT		
Note: Reference Oscillator must be re-adjusted when the radio screen is fitted and the temperature has stabilized at 27 Deg C. See 4.5.7, step 10					

4.5.4 UHF Receiver Front End Alignment

Step No	Result Measured by	Result Measured at	Adjust	Result	Notes
1			Switch on power and select channel 1.		Lowest freq. channel.
2		Antenna socket SK402	RF sig. gen. output..	50uV pd level and freq. for channel 1.	Modulate generator with 1 kHz at 60% of max. dev.
3	CRO, 5mV ac per div. 10uSec per div. 10x probe.	PIN 2 of U401	R554	Maximum level on CRO. Typ. 180mV p-p.	Sets tracking offset adjustment.
4			Select ch. 3		Highest freq. channel.
5			RF sig. gen. output.	Freq. of channel 3	
6	CRO 5mV ac per div 10uSec per div. 10x probe.	PIN 2 of U401	R557	Maximum level on CRC. Typ. 200mV p-p.	Sets tracking gain adjustment.
7 REPEAT STEPS 1 TO 6 TO ELIMINATE SLIGHT INTERACTION BETWEEN R554 AND R557.					
8			Select ch. 3		Highest freq. channel
g			RF sig. gen. output.	1 mV pd level, and freq. of channel 3.	
10	AF level meter.	Speaker output at S K202.	Volume control.	300mW in 4ohm.	
11	AF level meter.	Speaker output at SK202.	L404	Max. AF level.	Re-adjust volume for 300mW output when L404 is peaked
12	Distortion meter.	Speaker output at SK202.	L404	Less than 3%	Slight re-adjustment of L4'04 may be necessary
13			RF sig. gen. output.	0.31 uV pd level.	
14	SINAD meter	Speaker output at SK202.		Greater than 12dB SINAD.	Verifies alignment

4.5.5 VHF Receiver Front End Alignment

Step No	Result Measured by	Result Measured at	Adjust	Result	Notes
1			Switch on power and select channel 3.		Highest freq. channel.
2		Antenna socket SK403	RF sig. gen. output.	50uV pd., and freq. of ch. 3.	Modulate generator with 1 kHz at 60% of max. dev.
3	DVM, dc voltage range.	TP403	R557	16.0 +/- 0.5V	Sets tracking gain adjustment.
4	CRO, 5mV ac per div. 10uSec per div. 1 0x probe.	PIN 2 of	Tuning cores U401 FL401.	Max level of FL400 and	Sets tuning of filters. an CRO.
5			Select ch. 1		Lowest freq. channel.
6			RF sig. gen. output.	Freq. of channel l	
7	CRO, 5mV per div. l0uSec per div. 10x probe.	PIN 2 of U401.	R554	Max level on CRO.	Sets tracking offset adjustment.
8			Select ch. 3		Highest freq. channel.
g		Antenna socket SK402	RF sig. gen. output.	Freq. of channel 3	
10	CRO, 5mV per div. 10uSec per div. 1 0x probe	PIN 2 of U401	R557	Max level on CRO.	Slight re-adjustment may be necessary
11			RF sig. gen. output.	1 mV pd.	
12	AF level meter.	Speaker output at S K202	Volume control.	300mW in 4ohm.	
13	AF level meter.	Speaker output at SK202.	L404	Max AF level.	Re-adjust volume for 300mW output when L404 is peaked
14	Distortion Meter	Speaker output at SK202.	L404	Less than 3%.	Slight re-adjustment of L404 may be necessary

4.5.5 VHF Receiver Front End Alignment (Continued)

Step No	Result Measured by	Result Measured at	Adjust	Result	Notes
15			RF sig. gen. output.	0.31 uV pd level.	
16	SINAD meter	Speaker output at SK202.		Greater than 12dB SINAD.	Verifies alignment

4.5.6 Mute Maximum Alignment

Step No	Result Measured by	Result Measured at	Adjust	Result	Notes
1			Switch on power select channel 2.		Mid freq. channel.
2		Antenna socket SK402	RF sig. gen. output.	Freq. of ch. 2, 1 mV pd level	Modulate generator with 1 kHz at 60% of max dev.
3	AF level meter.	Speaker output SK202	Volume control.	300mW in 4ohm.	
4	Sinad meter	Speaker output SK202	RF sig. gen. output level	a) 23dB SINAD b) 19 +/- 1dB SINAD	a) for 20/25/30 kHz channel spacing b) for 12.5kHz channel spacing Record sig. gen. level.
5			Switch off RF sig. gen. output.		
6		Speaker output SK202	Mute control fully clock-wise.	AF should mute	If AF does not mute, adjust R455
7			Switch on RF sig. gen. Same output level as in step 4.	Ensure AF is muted.	If AF does not mute, adjust R455 slightly clockwise to achieve result.
8	AF level meter.	Speaker output SK202	R455 slowly counter-clockwise.	AF output Adjust R455 carefully appears.	
9	AF level meter.	Speaker output SK202	RF sig. gen. output off.	AF should mute If AF does not mute R455 has incorrect adjustment. Repeat steps 4 to 8.	
10	AF level meter.	Speaker output SK202	RF sig. gen. output on.	AF should If AF does not unmute. carefully re-adjust R455	

4.5.7 Transmit Modulation Alignment (No CTCSS)

Step No	Result Measured by	Result Measured at	Adjust	Result	Notes
1			Switch on power select ch.		Select ch.2 on VHF Select ch.3 on UHF
2		Microphone socket SK201 PIN 8	AF sig. gen. output	1 kHz at 400+/- 40mV rms	
3	CRO Vac per div. 0.5mSec per div. 1 x probe.	PIN 1 of SK400	Activate PTT Adjust 8316. Adjust R322.	Peak, approx 5V p.p.	Waveform should be square.
4	CRO, 5mV ac per div. 0.5mSec per d' 1 x probe.	TP401	R567	Null in amplitude typ. 1 mV p.p.	A stepped sine wave will be seen.
5	Deviation monitor.	Antenna socket SK402	R316	a)+/- 4.8kHz +0/-0.2 b)+/- 3.8kHz +0/-0.2 c)+/- 2.4kHz +0/-0.1	a) 25/30 kHz channel spacing b) 20kHz channel spacing c) 12.5kHz channel spacing
6	Deviation monitor.	Antenna socket SK402	AF sig. gen. output freq. 300Hz to 3kHz. Output level 400 +/- 40mV rms	Less than a)+/- 5.0kHz b)+/- 4.0kHz c) +/- 2.5kHz.	a) 25/30kHz channel spacing b) 20kHz channel spacing c) 12.5kHz channel spacing.
7			AF sig. gen. output.	1 kHz freq 40 +/- 4mV rms.	
8	Deviation monitor.	Antenna socket SK402	R322	a)+/- 3.0kHz +/- 0.2kHz b) +/- 2.0kHz +/- 0.2kHz c) +/- 1.5kHz +/- 0.1 kHz.	a) 25/30kHz channel spacing b) 20kHz channel spacing c) 12.5kHz channel spacing.
9			Disable PTT		
10	FIT RADIO SCREEN TO PRM80 UNDER TEST				
11			Activate PTT		
12		Microphone socket SK201 PIN 8.	AF sig. gen. output.	1 kHz at 400 +/- 40mV rms.	

4.5.7 Transmit Modulation Alignment (No CTCSS)(Continued)

Step No	Result Measured by	Result Measured at	Adjust	Result	Notes
13	Deviation monitor	Antenna socket SK402	R316	a)+/- 4.8kHz +0/-0.2 b)+/- 3.8kHz +0/-0.2 c)+/- 2.4kHz +0/-0.1	a) 25/30kHz channel spacing b) 20kHz channel spacing c) 12.5kHz channel spacing. Slight re-adjustment may be necessary
14			Disable PTT		

4.5.8 Transmit Modulation Alignment with CTCSS

Step No	Result Measured by	Result Measured at	Adjust	Result	Notes
1	Perform Alignment Procedure 4.5.7 Leave Radio Screen Fitted When Test Is Completed. Switch Off AF Signal. Generator..				
2			Switch on power select channel 6.		CTCSS test channel
3			Activate PTT		
4	Deviation monitor	Antenna socket SK402	R354	a)+/- 580Hz +/- 30Hz b) +/- 460Hz +/- 25Hz c)+/- 290kHz +/- 15Hz.	a) 25/30kHz channel spacing b) 20kHz channel spacing c) 12.5kHz channel spacing.
5		Microphone socket SK201	AF sig. gem. output.	1 kHz freq 400+/- 40mV rms	
B	Deviation monitor	Antenna socket SK402	R316	a)+/- 4.9kHz +0/-0.2 b)+/- 3.9kHz +0/-0.2 c)2.4kHz +0/-0.1	a) 25/30kHz channel spacing b) 20kHz channel spacing c) 12.5kHz channel spacing
7			Disable PTT		

4.5.9 TransmIt Modulation Alignment with Selcall

Step No	Result Measured by	Result Measured at	Adjust	Result	Notes
1	PERFORM ALIGNMENT PROCEDURE 4.5.7 (AND 4.5.8 IF CTCSS IS FITTED). SWITCH OFF A.F. SIG. GEN.				
2			Switch on power, select channel 5.		ch. 6 UHF ch. 5 VHF
3	LC Display		Press SEND button.		Checks display.
4	Deviation monitor	Antenna socket SK402	R323	a)+/- 4kHz +/- 200Hz b)+/- 3kHz +/- 200Hz c)+/- 2kHz +/- 100Hz	a) 25/30kHz channel spacing b) 20kHz channel spacing c) 12.5kHz channel spacing
5	Frequency counter at monitor	Antenna socket SK402		1358 +/- 4Hz..	
6					The selcall test will cease after 10 Secs. To i nterru pt the transmission the radio must be switched off.

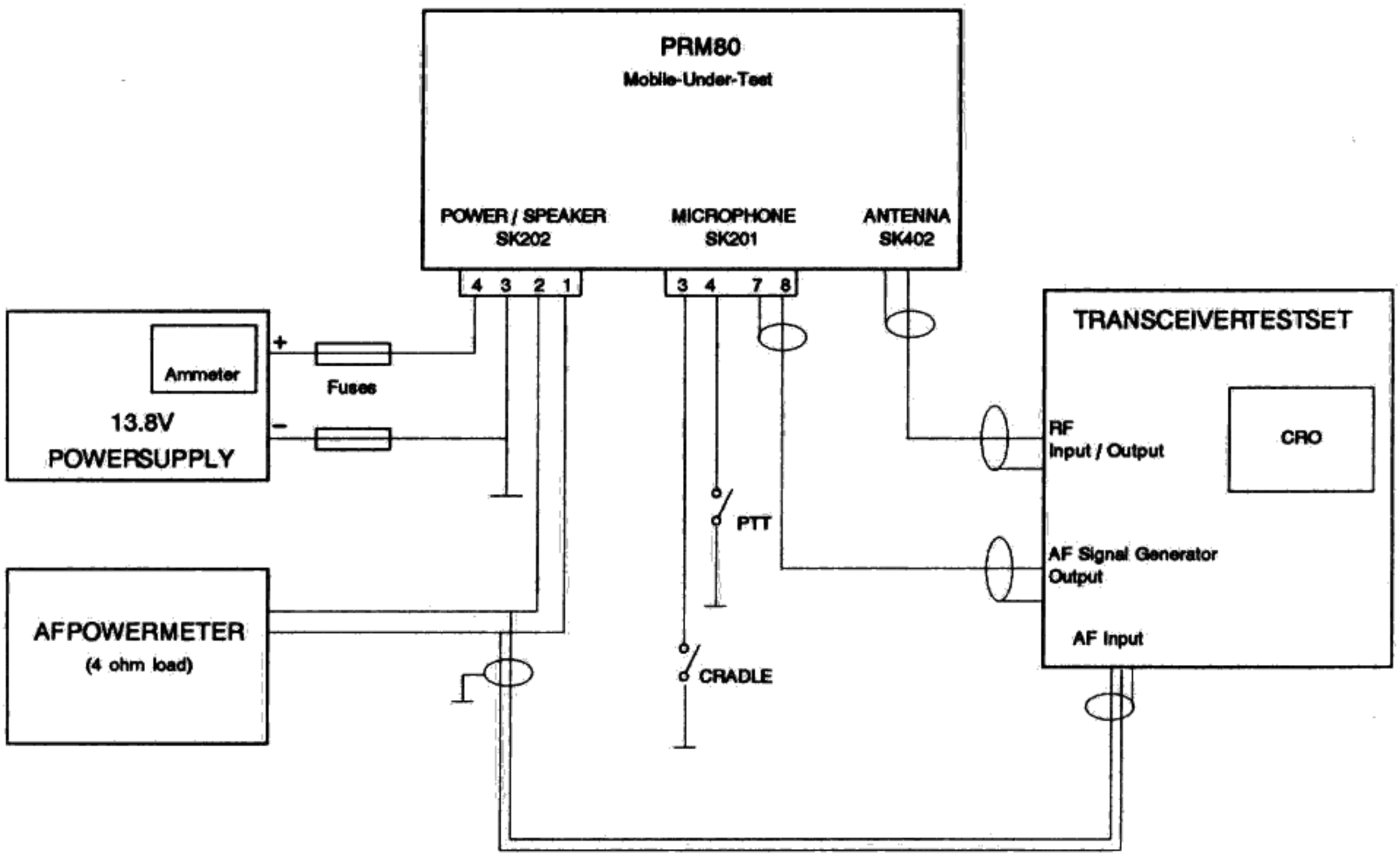


Figure 4.1 TEST EQUIPMENT SETUP

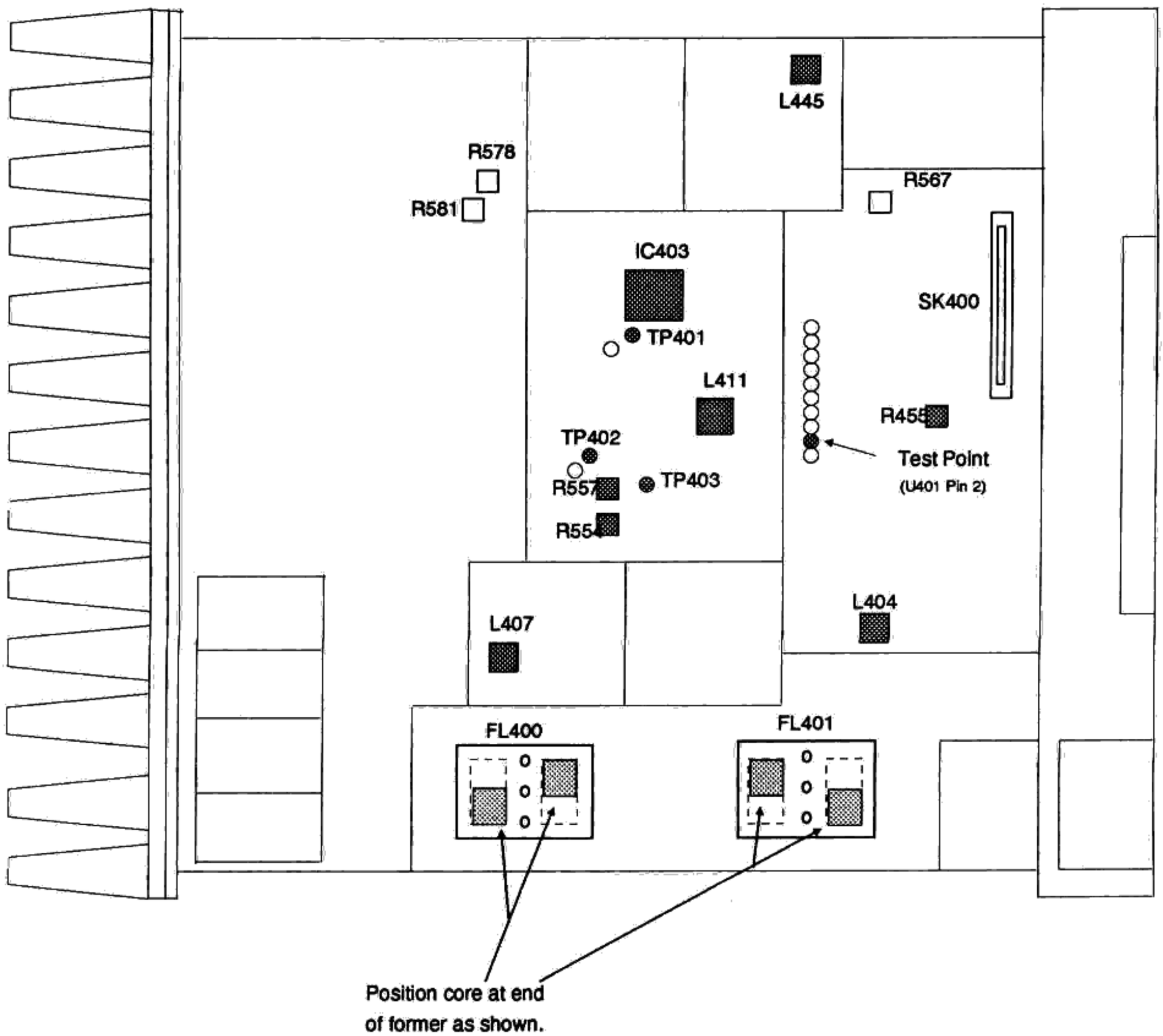


Figure 4.2 VHF RADIO PCB - ADJUSTMENT AND TEST POINT LOCATION DIAGRAM

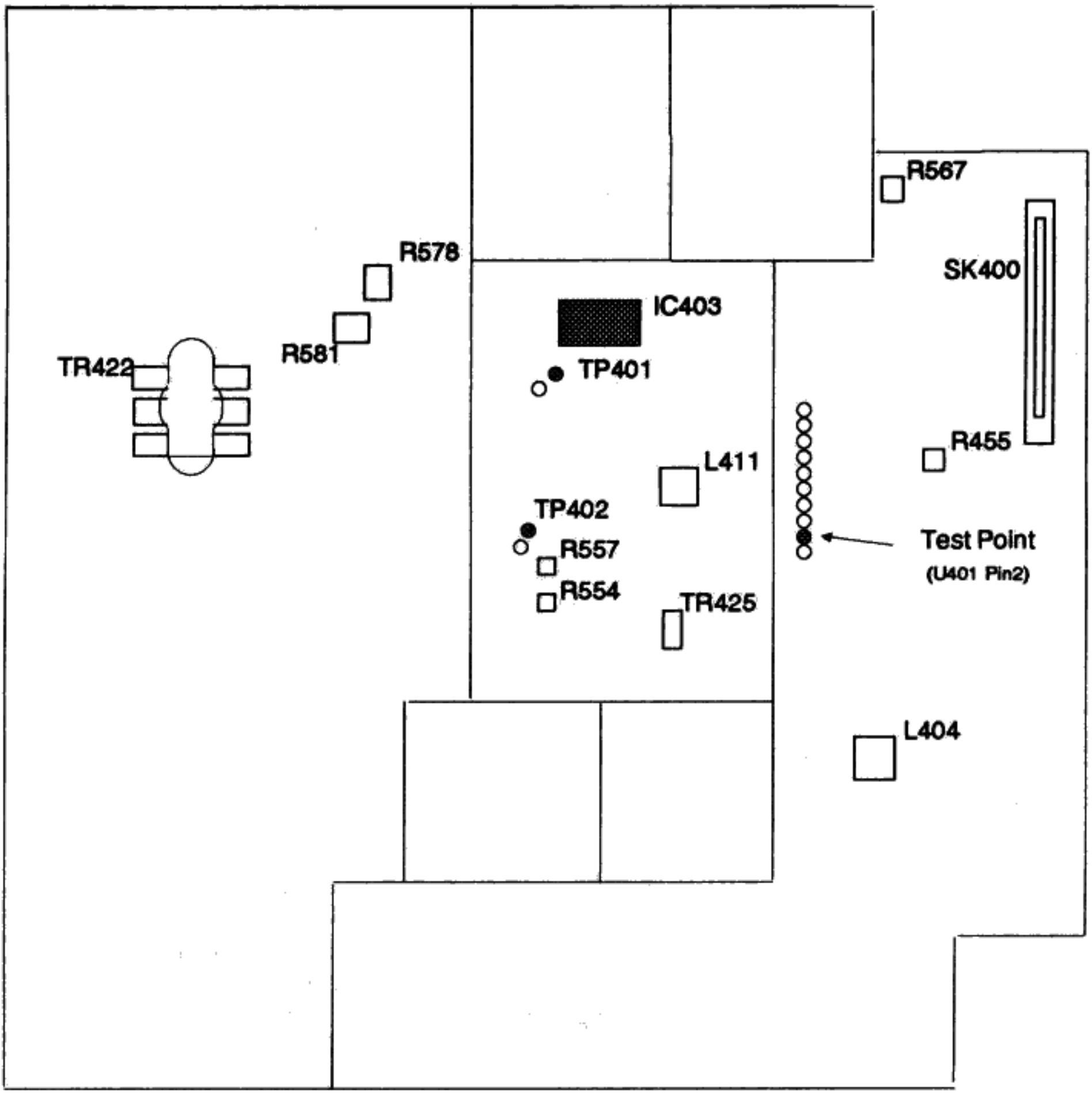


Figure 4.3

UHF RADIO PCB - ADJUSTMENT AND TEST POINT LOCATION DIAGRAM

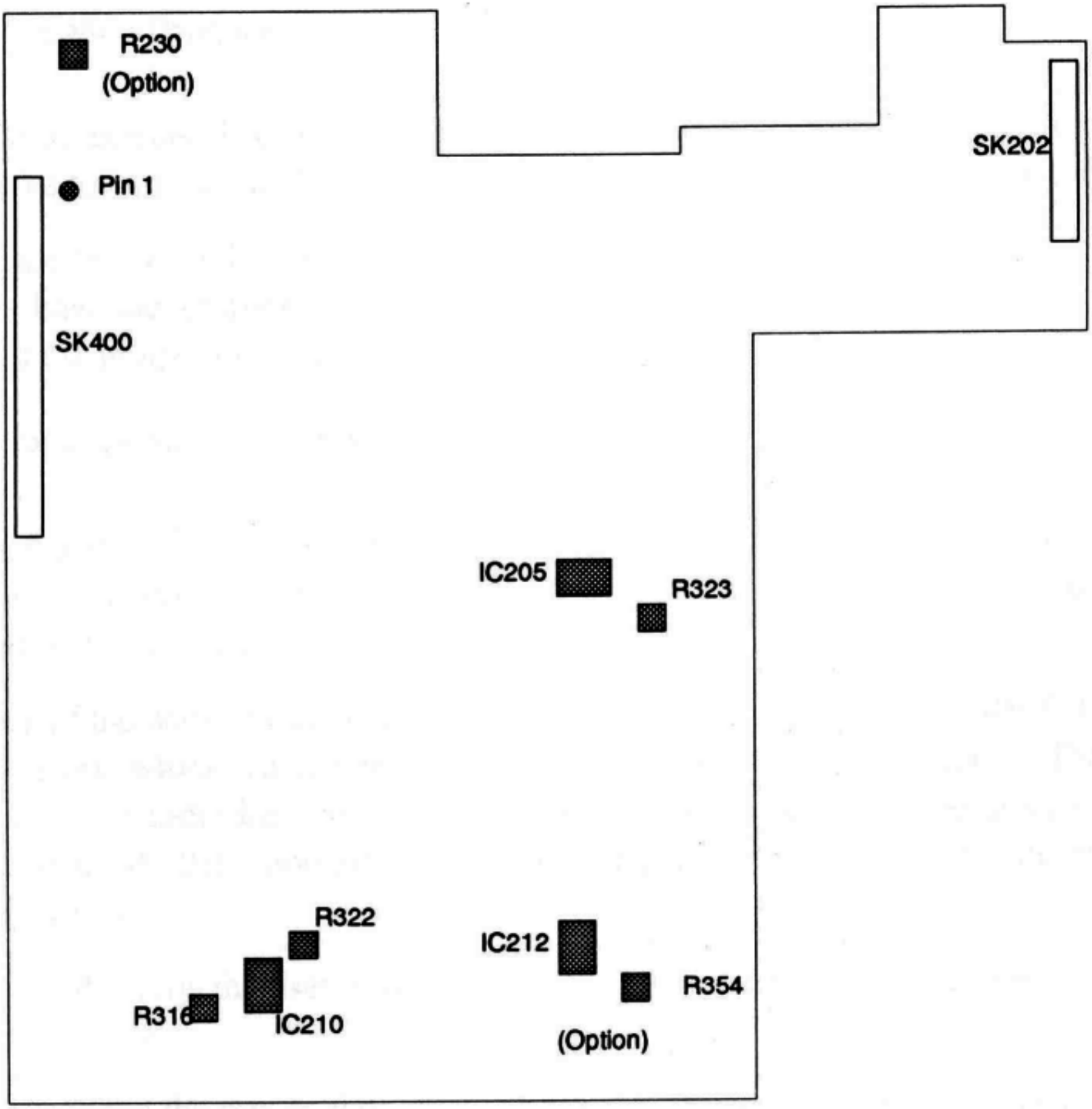


Figure 4.4

CONTROL PCB - ADJUSTMENT AND TEST POINT LOCATION DIAGRAM

SECTION 5 INSTALLATION INSTRUCTIONS

NOTE: Refer also to'"VEHICLE CARE" page at front of handbook

5.1 GENERAL INFORMATION

5.1.1 Operator Access

The mobile radio unit(s) must be fitted in such a position that the operator has easy access to the controls and the microphone when wearing a seat belt. The controls must also be situated so that they are within the driver's normal field of vision.

5.1.2 Location Dangers

Caution must be exercised before drilling holes through bulkheads to ascertain that it is safe to do so. Items to consider include fuel tank, fuel line, brake line, battery, cable loom etc.
Fitting the transceiver on the top of the dash is not recommended. Vehicles exposed to sunlight may have the temperature of the dash top rise to over 100 Deg C. Prolonged exposure to these temperatures may distort the plastic parts of the transceiver.

5.1.3 Vehicles Fitted With Electronic Devices

An additional precaution is necessary in relation to vehicles fitted with Electronic Ignition, Fuel Injection, Anti-skid Brakes or any other electronic device where temporary lass of service could be hazardous.

In theory, any of the above systems could be affected by the presence of an RF field of sufficient intensity, which when detected may cause the device to malfunction. The source of RF may be a mobile radio installed in the vehicle itself or a transmitter operating in another vehicle alongside. If interaction did occur, loss of control could result for the duration of the mobile transmission.

In the interests of safety, the user must be asked to test the vehicle when the installation is complete.

If a problem is found the owner should take the vehicle to an automobile specialist to resolve the problem. Unqualified persons should not attempt to modify these units in any way, the work should be done by a qualified automobile electrician.

5.1.4 Specialized Vehicles

The installation on certain specialized vehicles, such as Petrol Tankers and Fire Appliances, may be subject to safety regulations which must be closely observed.

Prior to commencing an installation on such a vehicle, be sure that any relevant safety regulations are fully understood.

5.1.5 Dash Mounted Equipment

Conditions in Section S.1.1 must be complied with when positioning equipment.

Fitting positions above the driver's or passenger's head must be avoided. Care should be taken to ensure that the microphone/handset lead is not installed such that the lead can interfere with the vehicle controls, or, with the driver's feet.

The microphone/handset clip should be fitted such that the microphone/handset is easily accessible. In the case of a loudspeaker it is necessary for the loudspeaker grill to face the operator when mounted.

The PRM80 series has been designed with safety in mind, e.g. non-reflective surface, no protrusions or sharp corners. Care must be taken when installing these, to ensure that any additional metalwork necessary to fix the units into the vehicle conforms to the same requirement.

Refer to Section 5.2 for mounting cradle and transceiver fitment detail.

5.1.6 Petrol Powered Vehicles

Ensure that there are no petrol leaks before commencing an installation involving the use of electric tools as these can produce sparks.

Ensure no damage to petrol tank or fuel lines occurs when drilling holes.

5.1.7 Gas Powered Vehicles

Before installation starts:

Establish that there are no gas leaks. DO NOT USE A FLAME. Butane and Propane are heavier than air, so if there is a leak the gas may lay on the floor of the boot. The gas is detectable by its characteristic smell. The point of escaping gas may show signs of frosting.

The vehicle owner should arrange for the leak to be repaired before the installation is commenced.

Ensure no damage to gas tank or gas lines occurs when drilling holes.

LT cables should be run, if possible, on the opposite side of the vehicle to the gas fuel pipe.

5.2 MAIN UNIT FITMENT

5.2.1 Cradle Installation

Refer to Figure 5.1.

Fit the transceiver cradle into the required position in the vehicle using a minimum of four screws. The screws should be placed as far apart from each other as possible. The base of the cradle is provided with slotted holes for situations where lateral adjustment is required during the installation.

Open ended holes are provided on the cradle at the transceiver mounting point. Ensure that these open ended holes are facing towards the rear of the transceiver, (away from the front panel location). The transceiver may be located in several planes of orientation, see figure 5.1; however it is not recommended to mount the transceiver onto a vertical surface so that the longitudinal axis of the transceiver is horizontal.

5.2.2 Transceiver Fitment

Refer to figure 5.2.

The transceiver is fitted into the cradle by guiding the fixed screws, located on the sides of the transceiver, into the open ended holes of the cradle. Two flat washers, two spring washers and two screws are then fitted through the cradle into the sides of the transceiver. Before finally securing these screws, the transceiver may be tilted for optimum display viewability and access to the front panel controls.

5.2.3 Transceiver Removal

The removal procedure of the transceiver from the cradle is simply the reverse of the procedure specified in section 5.2.2.

5.2.4 Microphone Installation

Refer to figure 5.3.

When the transceiver is installed in the cradle, the microphone may be fitted. Remove the microphone socket cover (if fitted).

NOTE: This item is supplied as a loose item when delivered as a standard packed unit from the factory.

The microphone may be plugged into the socket. A "click" should be heard which indicates that the locking mechanism has engaged. The microphone socket cover is fitted over the microphone socket by positioning the top edge of the cover approximately 10mm from top of the front panel. The cover will then fit into the front panel and appear flush with the front panel surface. The final requirement is to push the cover towards the top of the front panel until completely engaged and locked.

5.2.5 Microphone Removal

Refer to Figure 5.3.

To remove the microphone, first remove the microphone socket cover.

WARNING: This procedure requires that great care and precision be exercised when removing the cover so as to avoid causing damage to the plastic items.

A wide (10mm) flat blade screwdriver with a soft cloth fabric covering the blade is placed into the gap between the top of the cover and the front panel. Using a gentle lever action the cover is prised away from, and simultaneously pushed towards the bottom of, the front panel.

With the cover removed, the locldng tab on the top of the microphone plug is disengaged by using a 3mm flat blade screwdriver to press the tab towards the bottom of the front panel, and the microphone plug is withdrawn while this tab is being pressed.

5.2.6 Torque Settings for Retaining Screws

Use these settings to safeguard against damage to screws or threads.

Cover retaining screw (3502 310 44180) when cradle is used.

Knurled version	1 to 2 Nm	(8.85 to 17.7 lb ft ins)
Hexagon head version	2 to 2.5Nm	(17.7 to 22.1 lb ft ins)

Cover retaining screw (3502 310 44180) when cradle is not used.

	1 to 2 Nm	(8.85 to 17.7 lb ft ins)
All other retaining screws	1 to 2 Nm	(8.85 to 17.7 lb ft ins)

5.3 ANTENNA INSTALLATION

For best all round performance of the radiotelephone the antenna should be mounted on the centre of the vehicle roof. Alternative positions, such as guard mounted will give degraded performance.

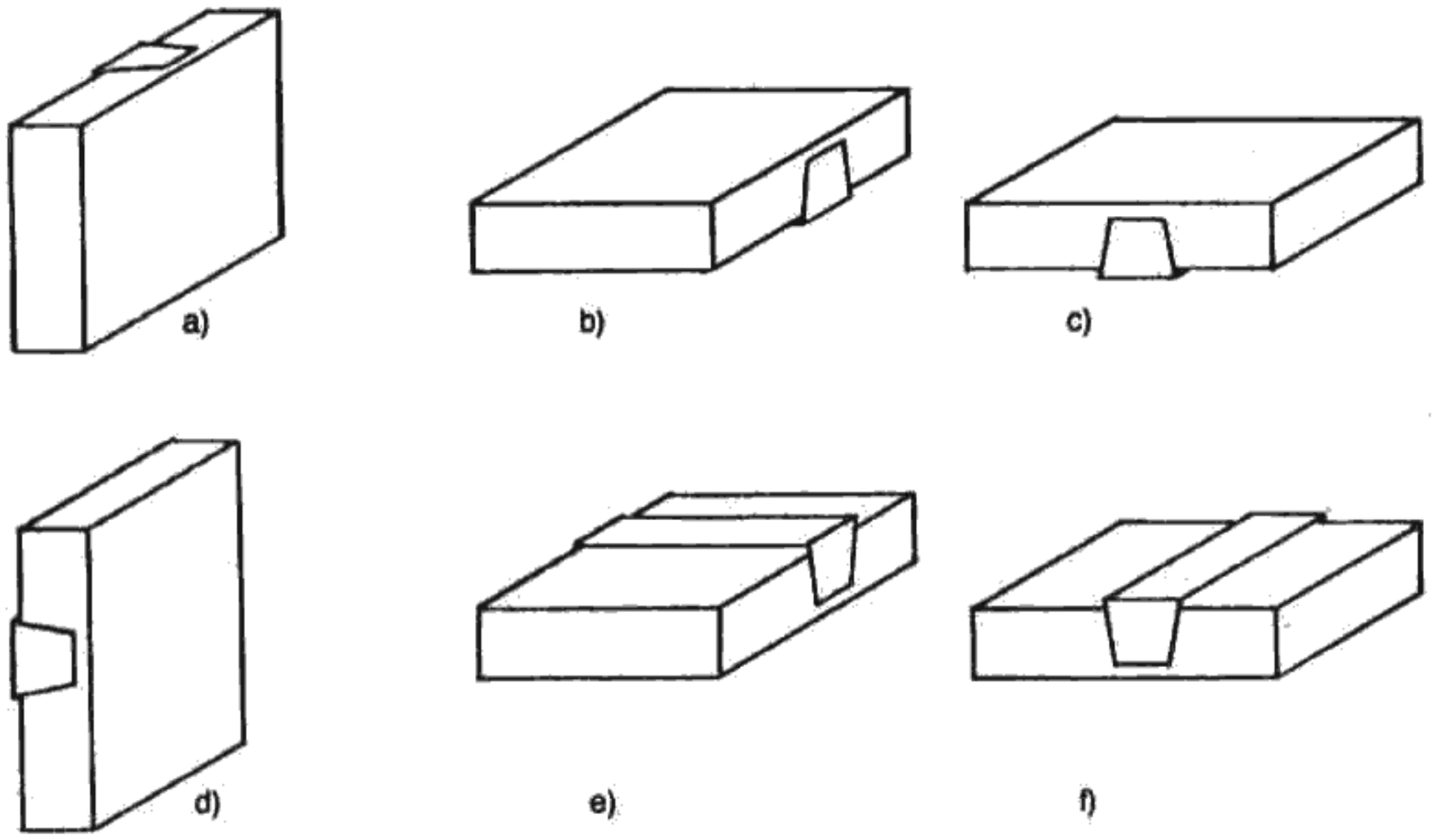
The coaxial feeder should be secured along its length to eliminate any possibility of damage by sharp edges or moving parts. Check the feeder for insulation and continuity.

5.4 DC SUPPLY CONNECTION

The radio supply should be connected to the vehicle battery as a continuous unbroken run, with the earth lead connected to the chassis end of the battery earth braid. This is to protect the radio equipment in the event of the battery becoming disconnected.

The leads contain in-ine fuse holders, and fuses of the correct rating must be fitted.

In the case of 24 volt do supply vehicles, an approved 24VI12V converter must be used. The supply should not be taken from a 12 volt tap on the battery supply.



a) On vertical surface
Not recommended.

b) and c) Above horizontal surface

d) On vertical surface

e) and f) Below horizontal surface

Figure 5.1 TRANSCEIVER / CRADLE - ORIENTATION DETAIL

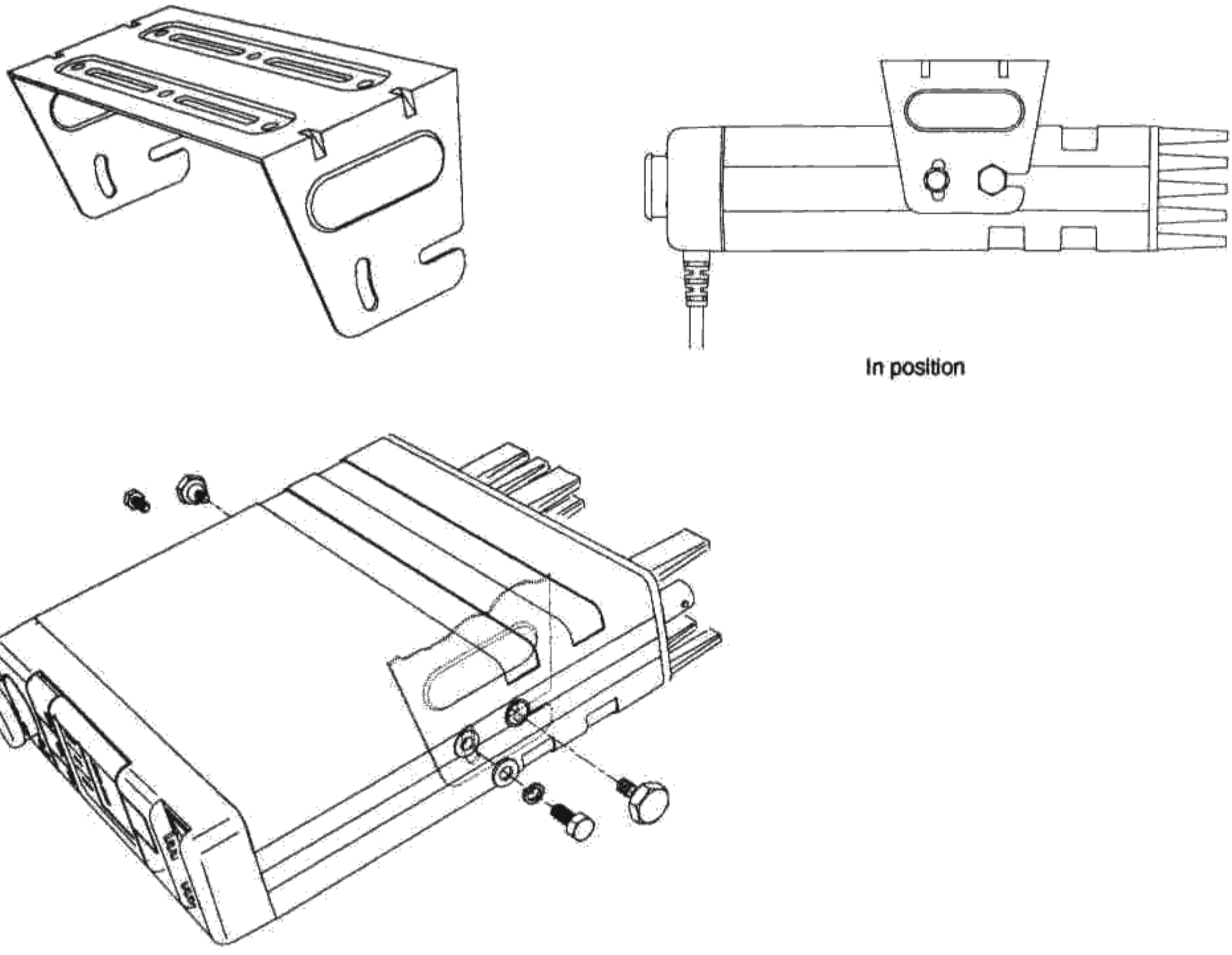


Figure 5.2 TRANSCEIVER / CRADLE - ASSEMBLY DETAIL

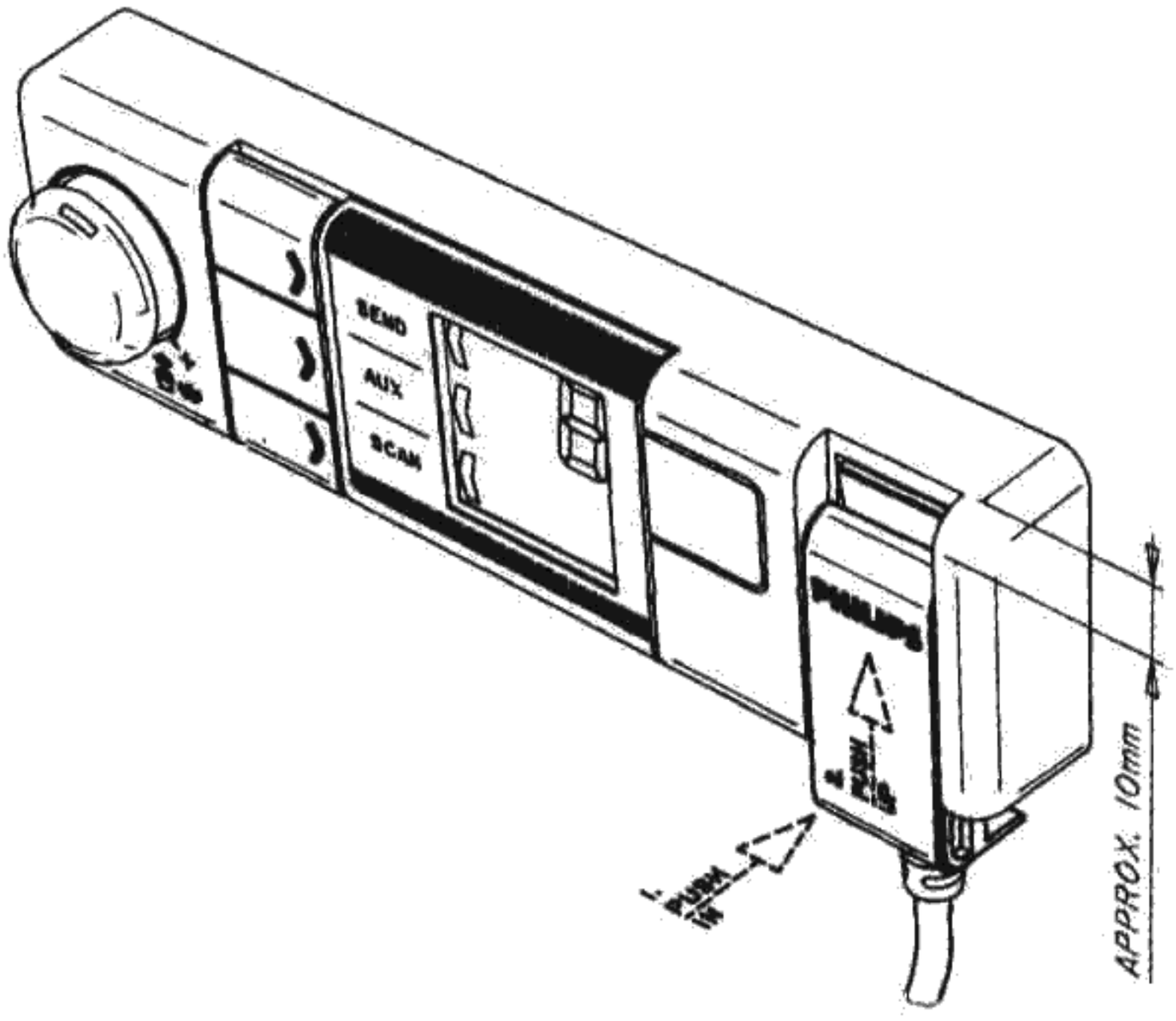


Figure 5.3 MICROPHONE COVER - ASSEMBLY DETAIL